



1981 CRC ALTITUDE OCTANE REQUIREMENT PROGRAM

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December 1981

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COORDINATING RESEARCH COUNCIL

INCORPORATED

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1981 CRC ALTITUDE OCTANE REQUIREMENT PROGRAM

(CRC PROJECT No. CM-124-81)

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Prepared by the

1981 Altitude Octane Requirement Program Analysis Panel

of the

CRC Road Test Group

December 1981

Light-Duty Vehicle Fuel, Lubricant, and Equipment Research Committee

of the

Coordinating Research Council, Inc.

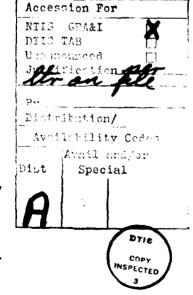


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I. SUMMARY

The last CRC altitude octane program was run in 1977. Since then, vehicle designs have changed substantially. In particular, many of the 1981 models are equipped with electronic systems for controlling air-fuel mixture and spark timing. Consequently, this program was run to determine the effect of altitude on octane requirements of 1981 cars with electronic control systems and to provide data for ASTM to consider for possible revision of the D 439 altitude octane specifications for gasoline. The results from this program are summarized as follows:

- Octane requirement tests were conducted in Denver, Colorado, at an elevation of 5,280 feet above sea level; and again in Los Angeles, California, at an elevation of 325 feet. Seventy-six cars were tested at each location. There were seven groups of ten cars each; two groups had barometrically compensated spark timing, and five did not. Six other cars also had barometric spark compensation, and three of those cars had knock sensors. All cars had closed-loop electronic control of air-fuel mixtures. Maximum octane requirements were determined with unleaded average sensitivity full-boiling range (FBRU) reference fuels and with unleaded high sensitivity full-boiling range (FBRSU) reference fuels. In addition, 50th percentile acceleration technique octane requirements were determined with FBRU fuels.
- The average octane requirements (raw and temperature-humidity corrected data) are summarized as follows:

| | | Octane Req. Los Angeles | | (RON)** Denver | | Difference (RON) | | Δ0NR/1000 ft. (RON) | |
|--|--------------------------------------|----------------------------|----------------------|----------------------|----------------------|---------------------|-------------------|------------------------|-------------------|
| | | Raw | Corr. | Raw | Corr. | Raw | Corr. | Raw | Corr. |
| 50 Cars without Spark Timing Compensation | FBRU Max. FBRU 50%* FBRSU Max. | 91.6 91.5 92.7 | 91.2 91.1 92.3 | 83.4 82.8 84.8 | 83.9 83.2 85.2 | 8.2 8.7 7.9 | 7.3 7.9 7.1 | 1.7 1.8 1.6 | 1.5 1.6 1.4 |
| 20 Cars with Spark Timing Compensation | FBRU Max. FBRU 50%* FBRSU Max. | 92.4 91.4 93.8 | 92.0 91.0 93.4 | 89.2 88.8 90.6 | 89.5 89.0 90.8 | 3.2 2.6 3.2 | 2.5 2.0 2.6 | 0.6 0.5 0.6 | 0.5 0.4 0.5 |

- For the cars with knock sensors in addition to spark compensation, the reductions in octane requirements with increasing altitude were similar to those shown above for the twenty cars with spark compensation alone.
- With FBRU fuels, the reduction in maximum octane requirements (raw data) per 1,000 feet increase in elevation for 1981 cars without spark compensation (1.7 RON) was between the average reductions observed for 1977 cars (1.1 RON) and 1971-1972 cars (1.9 RON). However, the reduction for 1981 cars with spark compensation (0.6 RON) was about one-half as much.

^{* 50%} refers to the 50th percentile acceleration technique.

^{**} Research Octane Number

II. INTRODUCTION

The last CRC altitude octane program was conducted in 1977. It was found that the octane requirements of vehicles decreased substantially at high altitude compared with the requirements at sea level. In the past, octane requirements of engines have decreased with increasing altitude, primarily because of three factors: carburetor enrichment; less vacuum spark advance (weaker vacuum signal); and reduced charge density with decreasing barometric pressure. Accordingly, gasolines sold in high-altitude locations may have lower octane quality than those sold at sea level. Many of the 1981 model vehicles are equipped with electronic systems for controlling air-fuel mixture and spark timing, and the use of such systems may become more common in future model years. With these systems, air-fuel mixtures at partthrottle are controlled near stoichiometric regardless of altitude, and spark timing may be advanced as barometric pressure decreases. It was anticipated, therefore, that octane requirements of 1981 vehicles may not decrease as much with increasing altitude as had been observed with previous model cars.

This program was run to determine the effect of altitude on octane requirements of 1981 cars, particularly those with electronic control of air-fuel mixture and spark timing, and to provide technical data for ASTM (American Society for Testing and Materials) to consider for possible adjustment of the D 439 altitude octane specifications for gasoline.

Representatives from eleven companies, listed in Appendix A, participated in the test program. This report was prepared by the CRC Altitude Octane Requirement Program Analysis Panel of the CRC Road Test Group, membership of which is listed in Appendix B. The detailed test program is included in Appendix C.

III. CARS TESTED

A. Selection

Selection of the vehicles for this test program was based on the availability of vehicles in Los Angeles and Denver. Selected models encompassed expected future electronic engine controls that are currently available on some models, including: feedback air-fuel control; electronic spark timing; and barometrically compensated spark timing. Eight 1981 models were chosen, and all but six vehicles, which were supplied by the manufacturer, were obtained from rental agencies. All but eight cars had accumulated at least 6,000 miles prior to the test program.

The following models were tested:

| Sample Size | Car Model | Engine | Engine Controls | | | | | |
|----------------|---|------------|----------------------|--|--|--|--|--|
| 10 | Buick Skylark | 2.5L - 2V | CLAF, EST | | | | | |
| 10 | Buick Skylark/ Oldsmobile Omega | 2.8L - 2V | CLAF, EST | | | | | |
| 10 | Buick Regal/ Oldsmobile Cutlass | 3.8L - 2V | BARO, CLAF, EST | | | | | |
| 3 | Buick Electra/ Cadillac Fleetwood | 4.1L - 4V | BARO, CLAF, EST, ESC | | | | | |
| 3 | Buick Riviera/ Cadillac El Dorado/ Oldsmobile Toronado | 4.1L - 4V | BARO, CLAF, EST | | | | | |
| 10 | Dodge Aries | 2.2L - 2V | CLAF, EST | | | | | |
| 10 | Lincoln/Mark VI | 5.OL - TBI | BARO, CLAF, EST | | | | | |
| 10 | Mercury Capri | 2.3L - 2V | CLAF | | | | | |
| 10 | Toyota Corolla | 1.8L - 2V | CLAF | | | | | |
| | NOTE: BARO = Barometrically Compensated Spark Timing CLAF = Closed-Loop Air-Fuel Control EST = Electronic Spark Timing TBI = Throttle Body Injection ESC = Electronic Spark Control with Knock Sensor | | | | | | | |

B. Preparation and Instrumentation

All vehicles were instrumented with a vacuum gauge and auxiliary fuel supply lines. Idle speed and spark timing were checked and reset to manufacturer specifications when necessary. Additional details concerning car preparation are contained in the test technique.

IV. REFERENCE FUELS

Octane requirements were measured at both altitudes using the FBRU and FBRSU series of 1981 CRC unleaded full-boiling range fuels. Average laboratory octane number ratings and blending data for these fuels are shown in Tables D-I and D-II of Appendix D. Inspection and composition data furnished by the fuel supplier are shown in Tables D-III and D-IV, respectively.

A. Unleaded Average Sensitivity Full-Boiling Range (FBRU) Reference Fuels

FBRU fuels were prepared from three base blends (RMFD 332-81, RMFD 333-81, and RMFD 334-81) in two octane number increments from 78 to 84 RON, and in one octane number increments from 84 to 100 RON.

B. Unleaded High Sensitivity Full-Boiling Range (FBRSU) Reference Fuels

FBRSU fuels were prepared from three base blends (RMFD 335-81, RMFD 336-81, and RMFD 337-81) in two octane number increments from 78 to 84 RON, and in one octane number increments from 84 to 101 RON.

V. TEST TECHNIQUE

Octane requirements were determined according to procedures outlined in the CRC E-15-81 technique (Appendix C, Attachment 1). Incidence of knock on tank fuel was not investigated, and octane requirements over the speed range on Primary Reference (PR) fuels were not determined in this program. Vehicle testing was conducted in the following sequence:

- Octane requirements of all seventy-six cars were determined in Denver, Colorado.
- 2. After requirements were determined in Denver, all cars were transported by truck to Los Angeles, California.
- 3. Octane requirements were determined in Los Angeles.

VI. TEST FACILITIES

The sea-level portion of the program was based at the Union Oil Research Center in Brea, California; and vehicle tests were conducted on Santa Ana Canyon Road in Anaheim, California, at an elevation of 325 feet.

The high-altitude tests were conducted in Denver, Colorado, at an elevation of 5,280 feet. Vehicle tests were run on Smith Road, which was used for the 1977 program; and the General Motors Vehicle Emissions Test Facility was used as the base of operations.

VII. WEATHER CONDITIONS

Ambient weather conditions were recorded for each octane rating. The range and mean values of barometric pressure, absolute humidity, and ambient temperature for each car group are listed in Appendix E, Tables E-I, E-II, and E-III, respectively. A summary of these data for all cars is as follows:

| | Barometr | ic Pressure, | in.Hg |
|---|----------------|-------------------------------|----------------|
| | <u>Hi gh</u> | Low | Mean |
| Los Angeles ⁽¹⁾ Denver ⁽²⁾ | 29.73 24.80 | 29.42 24.53 | 29.65 24.68 |
| | | olute Humidit s H2O/lb Dry | |
| | <u> High</u> | Low | Mean |
| Los Angeles Denver | 92 96 | 26 52 | 68 76 |
| | Ambien | t Temperature | , °F |
| | Hi gh | Low | Mean |
| Los Angeles Denver | 110 95 | 68 68 | 88 80 |

VIII. DISCUSSION OF RESULTS

A. General

Octane number requirements of individual cars determined in Los Angeles and in Denver are tabulated in Appendix F. For analysis, the test-car fleet was subdivided into seven groups of ten <u>similar</u> cars each. Each group of cars represented a specific vehicle and/or engine design. An eighth group of six cars was analyzed, and is treated separately.

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^{(1) 325} feet above sea level.

^{(2) 5,280} feet above sea level.

Because temperature and humidity varied widely between Los Angeles and Denver, all raw data were corrected to standard conditions of 70°F and 50 grains of humidity. Octane number requirements (ONR) were corrected by the following formula:

Corrected ONR = ONR measured + 0.054 (70 - T) - 0.035 (50 - H)

Where T and H are the temperature (°F) and humicity $\cdot gr$ observed when the octane requirement was measures.

Temperature and humidity coefficients, 0.054 $ON/^{\circ}F$ and 0.035 $ON/^{\circ}gr \sim_2 O$, were adopted from Section A.1.3.6 of the 1981 ASTM D 439 Automotive Gasoline Specifications. ONR values of 1981 cars were not corrected for variations in barometric pressure because:

- (1) the variation in barometric pressure in both Los Angeles and Denver during the 1981 program was small (\pm 0.3 inches Hg); and
- (2) the difference between the average barometric pressure in Los Angeles and Denver approximated the standard atmospheric pressure lapse rate; i.e., 1.0 inch Hg per 1,000 feet of altitude.

Both uncorrected and corrected octane requirements of individual cars are summarized in Appendix G.

B. Octane Number Requirements in Los Angeles vs. Octane Number Requirements in Denver

1. Car Groups 1-7

Individual car group raw and weather-corrected data were averaged for both Los Angeles and Denver. The data are summarized for maximum and 50th percentile acceleration technique requirements with FBRU fuel (Tables I and II) and for maximum requirements with FBRSU fuel (Table III). In addition to the individual car groups, averages for compensated cars (barometrically compensated spark timing - Groups 2 and 4) and non-compensated cars (Groups 1, 3, 5, 6, and 7) are also shown

Using the FBRU maximum requirement data, the mean octane requirement for non-compensated cars was 8.2 RON (7.3 RON weather-corrected) higher in Los Angeles than in Denver, while the compensated cars only differed by an average of 3.2 RON (2.5 RON weather-corrected).

Except as noted, all octane requirement differences were statistically significant at the 95 percent confidence level. The lesser change in octane requirements for the compensated cars is illustrated in Figure 1 for maximum and 50th percentile acceleration technique requirement conditions. This figure also shows that the change attributable to altitude is approximately the same, independent of driving condition or sensitivity of the fuel. The weather-corrected data are shown in Figure 2.

Car-to-car variations within individual car groups for FBRU maximum requirements are illustrated in Figures 3 and 4. The data ranged from 2 RON (Group 4 - Denver) to 16 RON (Group 7 - Denver). Although octane requirements vary widely within some car groups, the effect of altitude can be ascertained because individual cars were rated in both Los Angeles and Denver. The differences in mean octane requirements for each car group (Los Angeles versus Denver) are statistically significant at the 95 percent confidence level.

2. Car Group 8

In addition to the seven groups of ten cars each, another group of six cars was tested. All six cars had the same basic engine with barometrically compensated spark timing. Three of these cars had ESC systems with knock sensors (Group 8B), and the other three (Group 8A) did not. Octane requirements with FBRU fuels are listed in Tables IV and V, and with FBRSU fuels in Table VI.

For the cars with knock sensors, the minimum, maximum, and E-15 octane requirements (described in Appendix C, Attachment 1) at Los Angeles are compared with those at Denver in Figure 5. The increase in altitude reduced average octane requirements approximately 2 to 4 RON on a raw-data basis, and 2 to 5 RON on a weather-corrected basis. These reductions are similar to those shown in Figures 1 and 2 for compensated cars.

For the companion cars without knock sensors, the E-15 octane requirements at Los Angeles are compared with those at Denver in Figure 6. The increase in altitude reduced average octane requirements approximately 8 to 9 RON on a raw-data basis, and 7 to 8 RON on a weather-corrected basis. These reductions were much larger than those observed with the knock sensor cars (Figure 5) or the other compensated cars (Figures 1 and 2). In fact, the reductions were similar to those for the non-compensated cars shown in Figures 1 and 2. Because these cars were equipped with barometrically compensated spark timing, this anomalous behavior was not expected and cannot be explained from these data.

The variations in FBRU requirements (E-15) within car groups 8A and 8B are shown in Figures 3 and 4. The cars with knock sensors (Group 8B) had requirements which varied 6 RON in Los Angeles and 10 RON in Denver. The differences in the means were not significant at

the 95 percent confidence level. Similarly, the cars without knock sensors (Group 8A) had requirements which varied 6 RON in Los Angeles and 1 RON in Denver, and the differences in the means were significant at the 95 percent confidence level.

C. <u>Distribution of Differences in Octane Number</u> Requirements for Cars Tested at Los Angeles and Denver

The distribution of differences for the raw data are shown in Figures 7 through 13. The differences were determined by subtracting the octane requirements measured at Denver from those measured at Los Angeles for each individual car. The mean and standard deviation were determined for the differences in each car group.

The mean was plotted at the 50th percentile, and the mean plus the standard deviation was plotted at the 84th percentile. Using this procedure, a line drawn through these two points assumes a normal distribution.

Each plot contains three lines: maximum requirement for FBRU and FBRSU fuels, and the 50th percentile acceleration technique requirement on FBRU fuels.

Data are not shown for car groups 8A and 8B because of the small sample sizes (only three cars per group), which precludes drawing mean ngful distribution curves.

D. Comparison of 1981 CRC Altitude Program With Previous Altitude Studies

Results from previous altitude programs are summarized in Table VII. All data are expressed as the change in ONR per 1,000 feet change in altitude (Δ ONR/1,000 feet). Since data from previous programs were not weather-corrected, only the raw data from the 1981 cars are listed in Table VII so valid comparisons can be made among the various programs.

The Δ ONR/1,000 feet for non-compensated 1981 model cars is 1.7 RON, or about the average ONR charge observed in cars tested in two previous CRC programs. The Δ ONR/1,000 feet for 1977 cars and 1971-1972 cars was 1.1 RON and 1.9 RON, respectively. The Δ ONR/1,000 feet for compensated cars, however, is only 0.6 RON, or about one-third to one-half the change observed in the two previous programs and with the non-compensated cars in the 1981 program.

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REFERENCES

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TABLES

AND

FIGURES

TABLE I

FBRU MAXIMUM REQUIREMENTS

CAR GROUPS 1-7

| | Raw Data | | | Weat | her-Corre | ected Data |
|---|--|--|---|--------------------------------------|--|---|
| Group | LA | Denver | Difference | LA | Denver | Difference |
| | | | <u>R</u> | <u>ON*</u> | | |
| 1 2 3 4 5 6 7 Avg, All Cars | 88.7 90.6 88.9 94.1 92.7 93.2 94.7 | 81.5 87.6 80.2 90.7 83.5 84.2 87.6 | | 87.7 93.5 92.0 93.4 94.8 | 81.9 87.8 80.8 91.1 84.4 84.7 87.5 | 6.3 2.6 6.9 2.4 7.6 8.7 7.3 |
| Avg. Compensated | 92.4 | 89.2 83.4 | 3.2 8.2 | 92.0 | 89.5 | 2.5 |
| | - | | (RON + | MON)/2* | | |
| 1 2 3 4 5 6 7 | 85.3 86.7 85.4 89.6 88.5 88.9 90.1 | 79.6 84.4 78.6 86.9 81.2 81.7 84.4 | 5.7 2.3 6.8 2.7 7.3 7.2 5.7 | 84.5 89.1 87.9 | 84.5 79.1 87.2 81.9 82.1 | 4.9 2.1 5.4 1.9 6.0 7.0 5.9 |
| Avg, All Cars Avg, Compensated Cars (2 & 4) | 87.8 88.2 | 82.4 85.7 | 5.4 2.5 | 87.5 87.9 | | 4.8 2.0 |
| Avg, Non- Compensated Cars (1,3,5,6, & 7) | 87.6 | 81.1 | 6.5 | 87.3 | 81.5 | 5.8 |

MON = Motor Octane Number

^{*} RON = Research Octane Number

TABLE II

FBRU 50TH PERCENTILE ACCELERATION TECHNIQUE REQUIREMENTS

CAR GROUPS 1-7

| | | Raw Da | a ta | Weat | her-Corre | ected Data |
|---|------------------------------|--|--|--|--------------------------------------|---|
| Group | LA | Denver | Difference | LA | Denver | <u>Difference</u> |
| | | | | <u>RON</u> | | |
| 1 2 3 4 5 6 7 | 92.8 92.9 93.4 94.6 | 79.7 87.0 79.7 90.5 82.8 84.4 87.3 | 8.5 3.0 8.8 2.3 10.1 9.0 7.3 | 87.8 89.8 87.3 92.2 92.1 93.5 94.7 | 90.8 83.7 84.9 87.2 | 7.5 |
| Avg , All Cars Avg , Compensated Cars (2 & 4) Avg , Non- Compensated Cars (1,3,5,6, & 7) | 91.4 | 84.5 88.8 82.8 | 7.0 2.6 8.7 | 91.1 91.0 91.1 | 89.0 | 6.2 2.0 7.9 |
| | | | <u>(RON</u> + | MON)/2 | | |
| 1 2 3 4 5 6 | 88.7 89.1 | 83.9 | 6.7 2.4 6.9 1.9 8.0 7.2 5.8 | 84.6 86.1 84.2 88.1 88.0 89.1 90.1 | 84.1 78.7 86.9 81.4 82.3 | 6.1 2.0 5.5 1.2 6.6 6.8 5.9 |
| Avg, All Cars Avg, Compensated Cars (2 & 4) | | 82.0 85.3 | 5.5 2.1 | 87.2 87.1 | | 4.9 1.6 |
| Avg , Non- Compensated Cars (1,3,5,6, & 7) | 87.6 | 80.6 | 7.0 | 87.2 | 81.0 | 6.2 |

TABLE III

FBRSU MAXIMUM REQUIREMENTS CAR GROUPS 1-7

| | | Raw Da | ata | Weat | her-Corr | ected Data |
|---|--|--|---|--|--|---|
| Group | LA | Denver | Difference | LA | Denver | Difference |
| | | | | <u>RON</u> | | |
| 1 2 3 4 5 6 7 | 89.9 92.4 90.1 95.2 93.5 94.3 95.8 | 82.6 89.2 82.0 91.9 84.9 85.8 88.5 | 7.3 3.2 8.1 3.3 8.6 8.5 7.3 | 89.5 92.2 88.9 94.6 92.7 94.5 95.9 | 83.0 89.4 82.6 92.2 85.8 86.3 88.4 | 6.5 2.8 6.3 2.4 6.9 8.2 7.5 |
| Avg, All Cars Avg, Compensated Cars (2 & 4) Avg, Non- Compensated Cars (1,3,5,6, & 7) | 93.8 | 86.4 90.6 84.8 | 6.6 3.2 7.9 | 92.6 93.4 92.3 | 86.8 90.8 85.2 | 5.8 2.6 7.1 |
| | | | (RON + | MON)/2 | | |
| 1 2 3 4 5 6 7 | 85.3 87.4 85.4 89.8 88.3 89.0 90.3 | 79.1 84.7 78.6 87.0 81.0 81.8 84.1 | 6.2 2.7 6.8 2.8 7.3 7.2 6.2 | 85.0 87.2 84.4 89.2 87.6 89.2 90.4 | 79.4 84.9 79.1 87.2 81.8 82.3 84.0 | 5.6 2.3 5.3 2.0 5.8 6.9 6.4 |
| Avg, All Cars Avg, Compensated | 87.9 | 82.3 | 5.6 | 87.6 | 82.7 | 4.9 |
| Cars (2 & 4) Avg, Non- | 88.6 | 85.8 | 2.8 | 88.2 | 86.0 | 2.2 |
| Compensated Cars (1,3,5,6, & 7) | 87.7 | 80.9 | 6.8 | 87.3 | 81.3 | 6.0 |

TABLE IV

FBRU REQUIREMENTS CAR GROUPS 8A AND 8B

| | | | Raw Dat | <u>a</u> | Weath | Weather-Corrected Data | | |
|-----|-----------|------|---------|------------|-------|------------------------|------------|--|
| Gro | oup | LA | Denver | Difference | LA | Denver | Difference | |
| | | | | | | | | |
| | | | ~ | <u>RON</u> | | | ~~~~ | |
| 8A | (E-15) | 90.7 | 81.7 | 9.0 | 90.2 | 82,1 | 8,1 | |
| 88 | (E-15) | 96.3 | 93.0 | 3.3 | 96.8 | 93.1 | 3.7 | |
| 88 | (Minimum) | 87.3 | 83,3 | 4.0 | 87.8 | 83.4 | 4.4 | |
| 8B | (Maximum) | 98.3 | 94.7 | 3.7 | 98.8 | 94.7 | 4.0 | |
| | | | | (RON + MO | N)/2 | | | |
| | | | | | | | | |
| A8 | (E-15) | 86.9 | 79.6 | 7.3 | 86.5 | 80.1 | 6.4 | |
| 88 | (E-15) | 91.3 | 88.7 | 2.6 | 91.7 | 88.8 | 2.9 | |
| 88 | (Minimum) | 84.2 | 81.0 | 3.2 | 84.6 | 81.1 | 3.5 | |
| 88 | (Maximum) | 93.0 | 90.1 | 2.9 | 93.7 | 90.0 | 3.7 | |

TABLE V

FBRU 50TH PERCENTILE ACCELERATION TECHNIQUE REQUIREMENTS

CAR GROUPS 8A AND 8B

| | | Raw Da | ı ta | Weat | Weather-Corrected 1 | | |
|--------------|------|--------|-------------------|------------|---------------------|------------|--|
| Group | LA | Denver | <u>Difference</u> | LA | Denver | Difference | |
| | | | | | | | |
| | | | <u>R</u> | <u>:ON</u> | | | |
| | | | | | | | |
| 8A (E-15) | 89.2 | 81.0 | 8.2 | 88.7 | 81.4 | 7.3 | |
| 8B (E-15) | 96.0 | 93.0 | 3.0 | 96.4 | 93.1 | 3.4 | |
| 8B (Minimum) | 87.0 | 82.7 | 4.3 | 87.4 | 82.7 | 4.7 | |
| 8B (Maximum) | 97.7 | 96.0 | 1.7 | 98.1 | 96.1 | 2.0 | |
| | | | / DON . | MON: \ /2 | | | |
| | | | <u>(RON +</u> | MUN) / 2 | | , | |
| 8A (E-15) | 85.8 | 79.0 | 6.8 | 85.4 | 79.4 | 6.0 | |
| 8B (E-15) | 91.0 | 88.7 | 2.3 | 91.4 | 88.8 | 2.õ | |
| 8B (Minimum) | 84.0 | 80.5 | 3.5 | 84.3 | 80.5 | 3.8 | |
| 8B (Maximum) | 92.5 | 91.0 | 1.5 | 92.8 | 91.1 | 1.7 | |

TABLE VI

FBRSU REQUIREMENTS

CAR GROUPS 8A AND 8B

| | | Raw Da | ıta | Weather-Corrected Data | | |
|--------------|------|--------|--------------|------------------------|--------|------------|
| Group | LA | Denver | Difference | LA | Denver | Difference |
| | | | | | | |
| | | | · <u></u> | <u> </u> | | |
| 8A (E-15) | 93.3 | 84.3 | 9.0 | 92.9 | 84.8 | 8.1 |
| 8B (E-15) | 97.0 | 95.0 | 2.0 | 97.4 | 95.1 | 2.4 |
| 8B (Minimum) | 86.3 | 84.0 | 2.3 | 86.8 | 84.1 | 2.7 |
| 8B (Maximum) | 99.7 | 97.0 | 2.7 | 100.1 | 97.1 | 3.0 |
| | | | (RON + | MON) /2 | | |
| | | | (<u>non</u> | 11011//2 | | |
| 8A (E-15) | 88.1 | 80.6 | 7.5 | 87.8 | 81.0 | 6.8 |
| 8B (E-15) | 91.3 | 89.6 | 1.7 | 91.6 | 89.7 | 1.9 |
| 8B (Minimum) | 82.3 | 80.3 | 2.0 | 82.7 | 80.4 | 2.3 |
| 8B (Maximum) | 93.6 | 91.3 | 2.3 | 93.9 | 91.4 | 2,5 |

COMPARISON OF RESULTS FROM 1981 CRC ALTITUDE PROGRAM WITH THOSE FROM PREVIOUS ALTITUDE PROGRAMS (RAW DATA)

TABLE VII

| | Ref* | | Cars | Reference | △ONR/ |
|------------------------------|------|--------------------|--|--------------------------------------|-------------------------------|
| Source | No. | No. | Model Year | <u>Fuel</u> | 1,000 Ft, RON |
| | | | | | |
| Ethyl | 1 | 5 | 1949 | FBR & PR | 2.4 |
| Exxon | 2 | 3 | 1954-1955 | PR | 2.8 |
| Amoco | 3 | 8 | 1961 | FBR | 1.2 |
| Chevron & Ethyl | 4 | 8 | 1965 | FBR & PR | 1.5 |
| 1972 CRC Altitude Program | 5 | 6 6 39 39 | 1967-1970 1967-1970 1971-1972 1971-1972 | AU-8 PR AU-8 PR | 1.2 1.2 1.9 1.7 |
| 1977 CRC Altitude Program | 6 | 24 | 1 977 1 977 | FBRU PR | 1.1 1.0 |
| | | | | | RON (R+M)/2 |
| 1981 CRC Altitude Program | | 50 | 1981 NC 1981 NC 1981 NC | FBRU Max. +FBRU 50% FBRSU Max. | 1.7 1.3 1.8 1.4 1.6 1.4 |
| | | 20 | 1981 C 1981 C 1981 C | FBRU Max. +FBRU 50% FBRSU Max. | 0.6 0.5 0.5 0.4 0.6 0.6 |

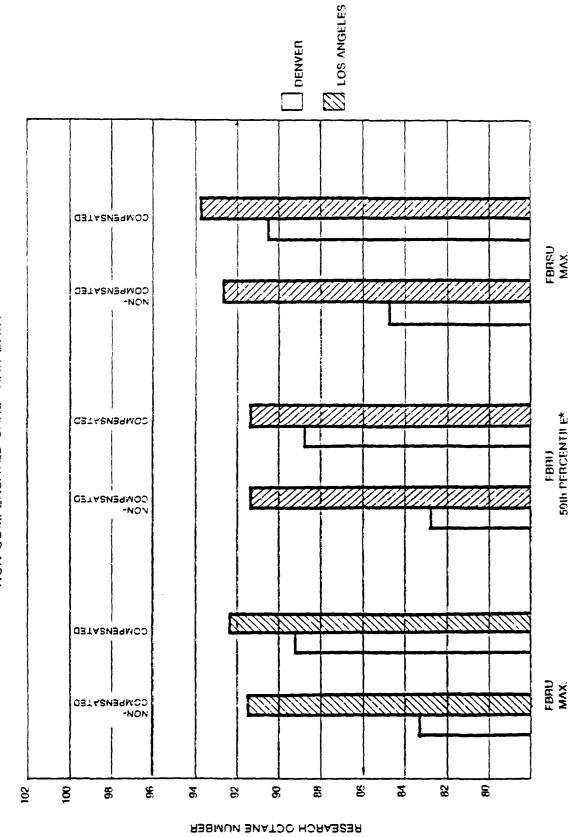
NC = Non-Compensated

C = Barometric Pressure Compensated Spark Timing

^{*}References listed on page 11 of this report.

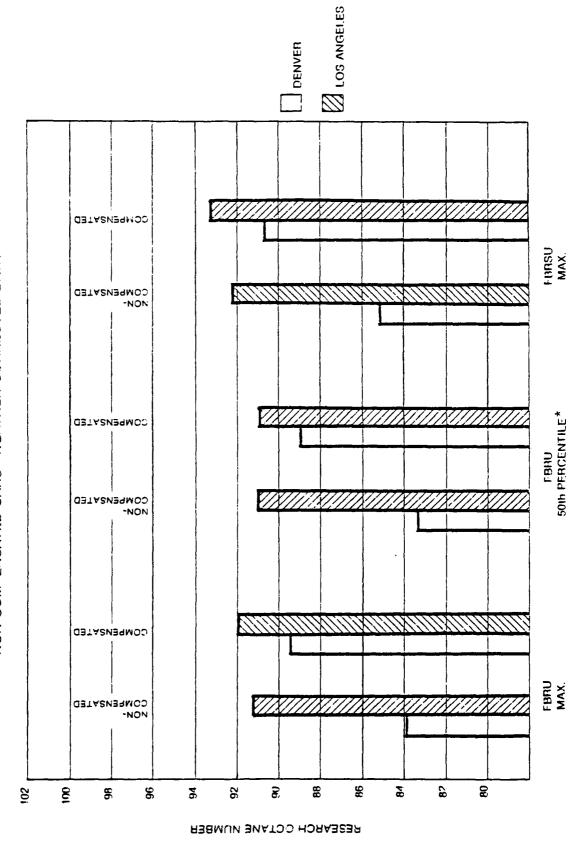
⁺⁵⁰th Percentile Acceleration Technique

AVERAGE OCTANE REQUIREMENTS OF COMPENSATED CARS COMPARED WITH THOSE OF NON-COMPENSATED CARS--RAW DATA



* 50th Percentile Acceleration Technique

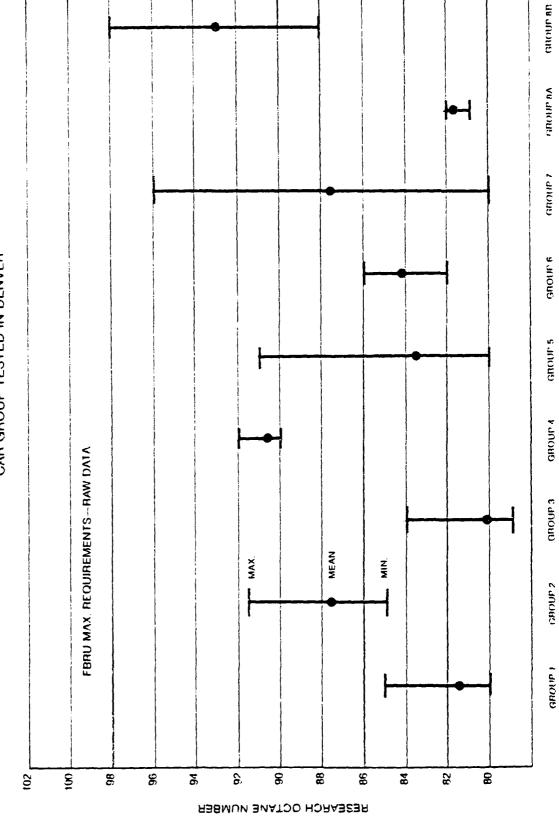
AVERAGE OCTANE REQUIREMENTS OF COMPENSATED CARS COMPARED WITH THOSE OF NON-COMPENSATED CARS... WEATHER-CORRECTED DATA



* 50th Percentile Acceleration Technique

FIGURE 3

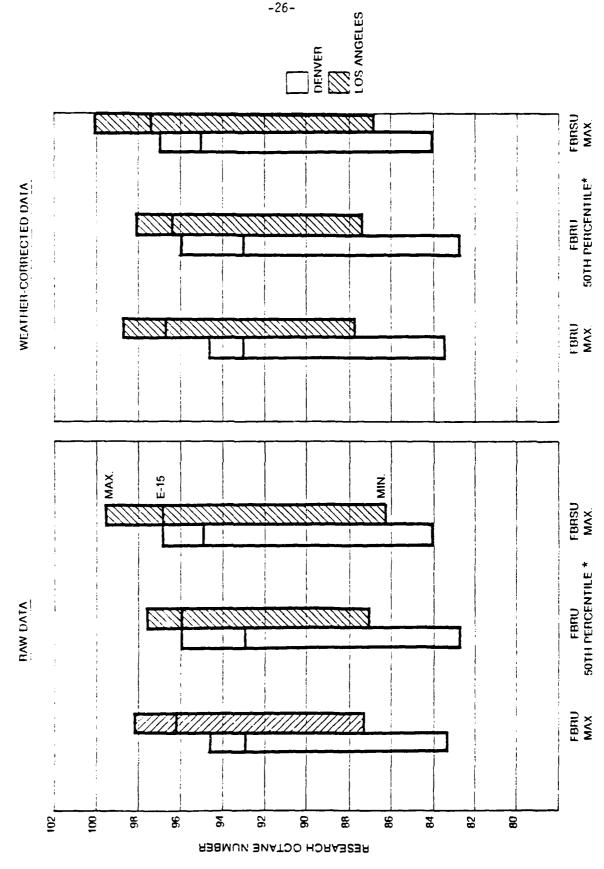
RANGE IN INDIVIDUAL OCTANE REQUIREMENTS WITHIN EACH
CAR GROUP TESTED IN DENVER



GROUP AR GROUP BA RANGE IN INDIVIDUAL OCTANE REQUIREMENTS WITHIN EACH CAR GROUP TESTED IN LOS ANGELES GROUP 7 SHOUP 6 GROUPS GROUP 4 FRRU MAX. REQUIREMENTS—RAW DATA GROUP 3 GHOUP 2 MEAN MAX Z GROUP ! 102 9 96 96 94 8 98 88 82 6 3 8 RESEARCH OCTANE NUMBER

FIGURE 4

AVERAGE OCTANE REQUIREMENTS OF GROUP 8B CARS EQUIPPED WITH KNOCK SENSORS FIGURE 5



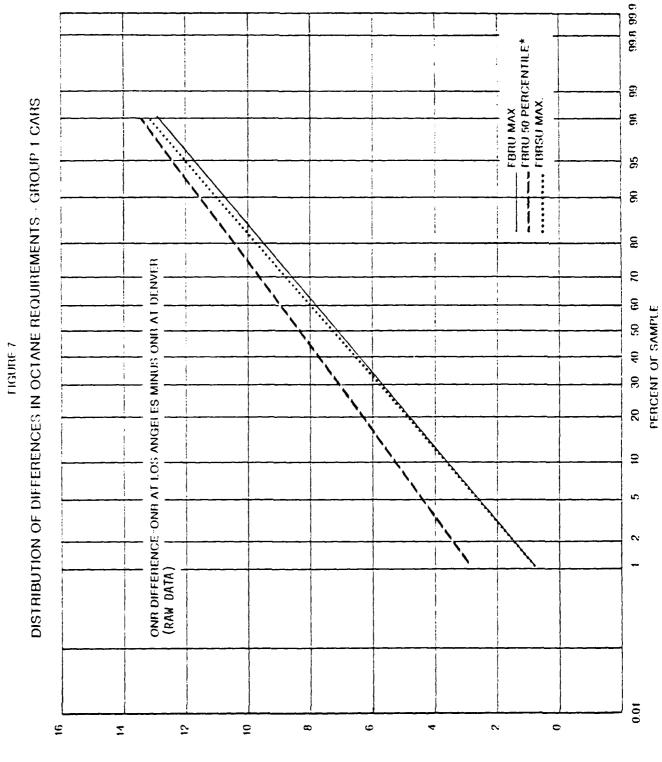
* 50th Percentile Acceleration Technique

DENVER

LOS ANGELES 50TH PERCENTILE * WEATHER-CORRECTED DATA AVERAGE OCTANE REQUIREMENTS OF GROUP 8A CARS NOT EQUIPPED WITH KNOCK SENSORS FIGURE 6 FBRSU Max. FBRU 50TH PERCENTILE * NAW DATA FBRIJ MAX. 102 5 96 94 92 8 98 8 82 98 8

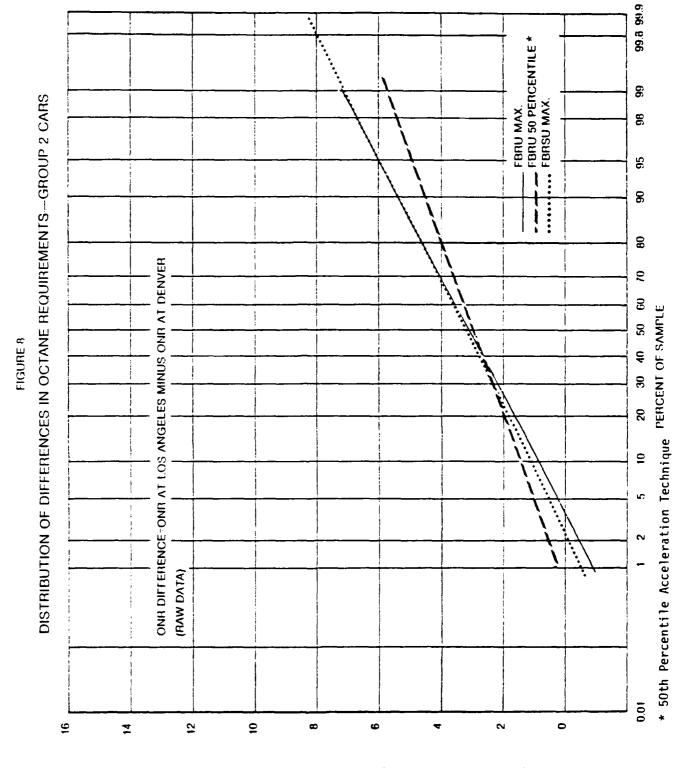
RESEARCH OCTANE NUMBER

50th Percentile Acceleration Technique

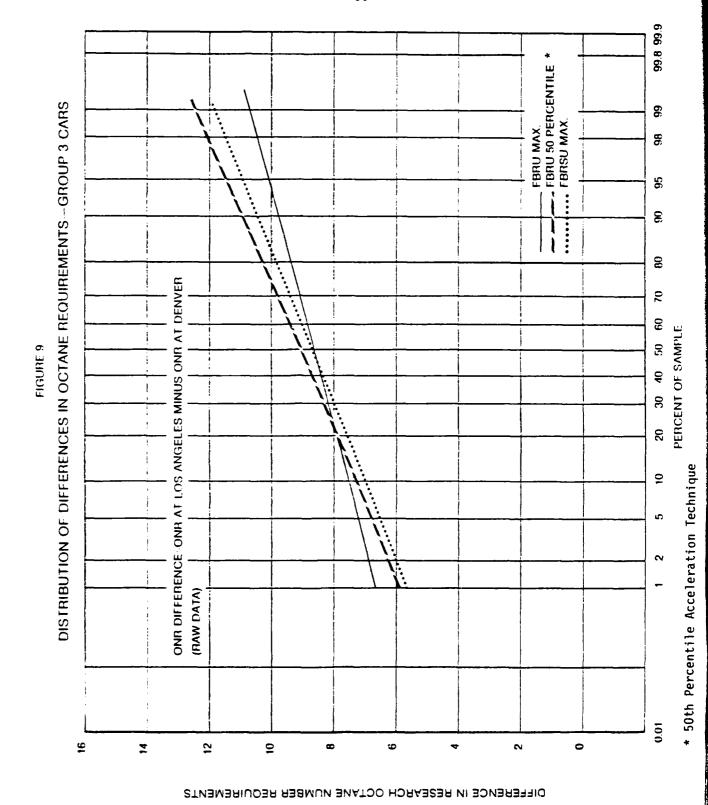


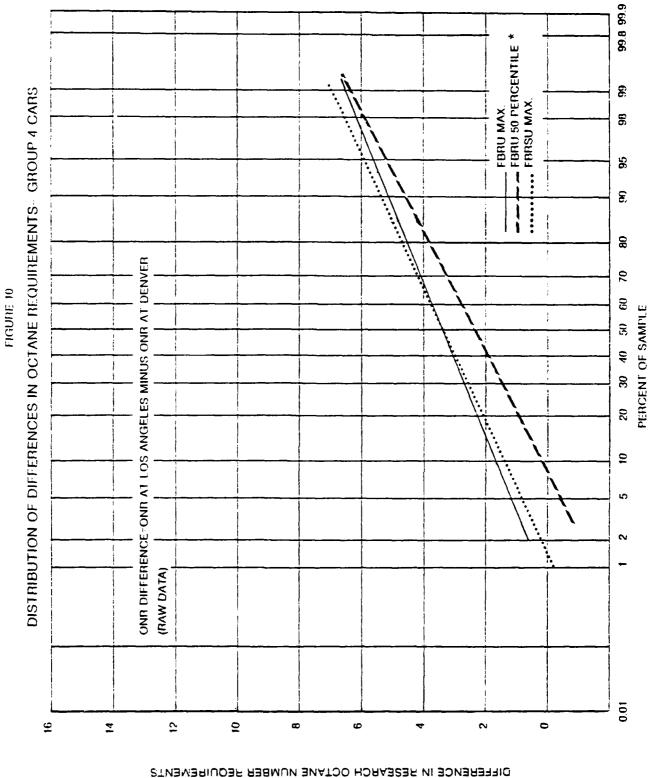
DIFFERENCE IN RESEARCH OCTANE NUMBER REQUIREMENTS

* 50th Percentile Acceleration Technique

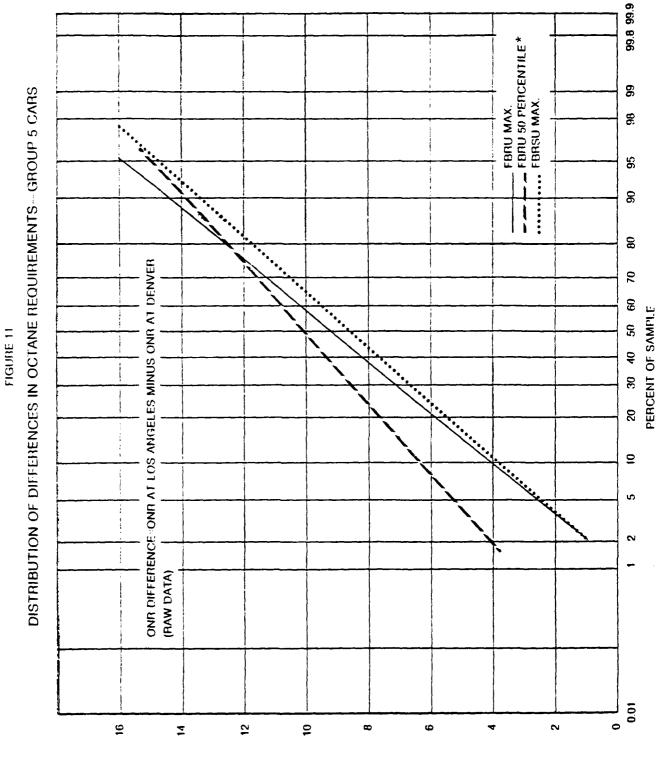


DIFFERENCE IN RESEARCH OCTANE NUMBER REQUIREMENTS





* 50th Percentile Acceleration Technique



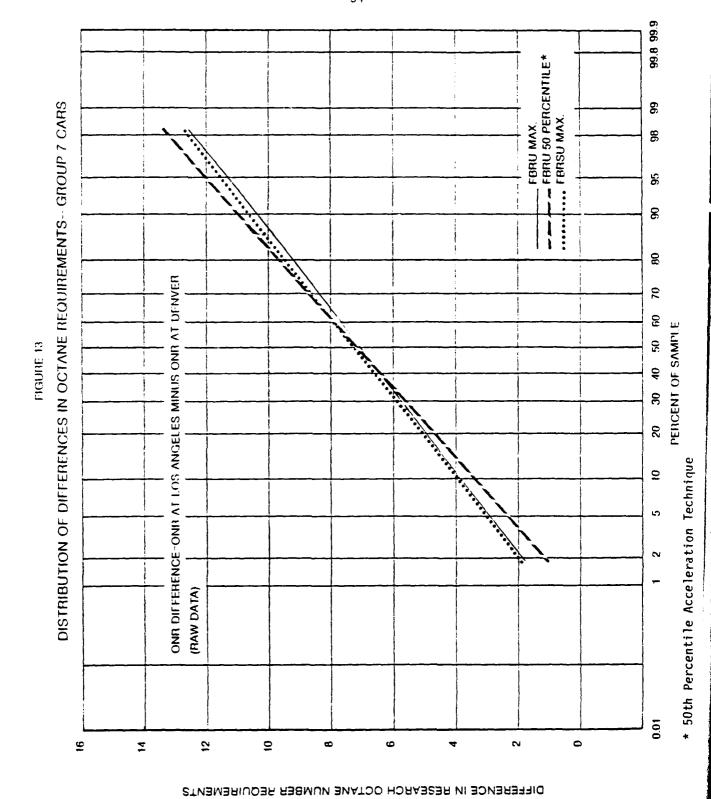
DIFFERENCE IN RESERBOH OCTANE NUMBER REQUIREMENTS

* 50th Percentile Acceleration Technique

99.8 99.9 FBRU MAX.
FBRU 50 PERCENTILE *
FBRSU MAX. 66 DISTRIBUTION OF DIFFERENCES IN OCTANE REQUIREMENTS-GROUP 6 CARS 98 95 8 8 ONR DIFFERENCE ONR AT LOS ANGELES MINUS ONR AT DENVER 2 50 60 PERCENT OF SAMPLE FIGURE 12 **ę** 30 2 ₽ (RAW DATA) 0.01 9 Ξ 9 8 9 ~ 8 12

DIFFERENCE IN RESEARCH OCTANE NUMBER REQUIREMENTS

* 50th Percentile Acceleration Technique



APPENDIX A

PARTICIPANTS

PARTICIPANTS

Amoco Research Center Naperville, Illinois

Chevron Research Company Richmond, California

Exxon Research and Engineering Company Linden, New Jersey

Ford Motor Company Dearborn, Michigan

General Motors Research Laboratories Warren, Michigan

Gulf Research and Development Company Pittsburgh, Pennsylvania

Marathon Research Center Denver, Colorado

Mobil Research and Development Corporation Paulsboro, New Jersey

Shell Development Company Houston, Texas

Standard Oil Company (Ohio) Cleveland, Ohio

Union Oil Company of California Brea, California

EQUIPMENT AND FACILITIES

General Motors Emission Test Facility

-- Garage facilities and base of operation in Denver, Colorado

Union Oil Research Center

-- Garage facilities and base of operation in Brea, California

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APPENDIX B

MEMBERSHIP: 1931 CRC ALTITUDE OCTANE REQUIREMENT
PROGRAM ANALYSIS PANEL

1981 CRC ALTITUDE OCTANE REQUIREMENT PROGRAM

(CRC Project No. CM-124-81)

1981 ANALYSIS PANEL

J. D. Benson, Leader General Motors Research Laboratories

P. W. Misangyi Ford Motor Company

J. B. Smith Amoco Research Center

T. Wusz Union Oil Company of California

APPENDIX C

1981 CRC ALTITUDE OCTANE REQUIREMENT
TESTING PROGRAM

COORDINATING RESEARCH COUNCIL

INCORPORATED

219 PERIMETER CENTER PARKWAY ATLANTA, GEORGIA 30346 (404) 396-3400

1981 CRC ALTITUDE OCTANE REQUIREMENT PROGRAM

CRC Project No. CM-124-81

Revised

January 1981

1981 CRC Altitude Octane Requirement Program

<u>Objectives</u>

The purpose of this work is to determine the effect of altitude on octane requirements of 1981 cars, particularly those with electronic control of air-fuel mixture and spark timing, and provide technical data for ASTM to consider for possible adjustment of the D-439 altitude octane specifications for gasoline.

<u>In</u>troduction

In 1977, CRC conducted an altitude octane program and found that octane requirements of vehicles (even those with altitude compensation) decreased substantially at high altitude compared to the requirements at sea level.

Many of the 1981 model cars will be equipped with electronic systems for controlling air-fuel ratio and spark timing, and the use of these systems may become more common in subsequent model years. In the past, octane requirements of engines have decreased with increasing altitude primarily because of three factors: carburetor enrichment, less vacuum spark advance (weaker vacuum signal), and reduced charge density with decreasing barometric pressure. Accordingly, gasolines sold in high altitude locations may have lower octane quality than those sold at sea level. However, with some of the 1981 cars, air-fuel mixtures at part-throttle are controlled near stoichiometric regardless of altitude, and spark timing may be advanced as barometric pressure decreases. Therefore, it is anticipated that octane requirements of these vehicles may not decrease as much with increasing altitude as has been observed with previous model cars.

This program is being proposed because both the oil companies and the automobile manufacturers are interested in satisfying the octane requirements of 1981 and future vehicles at high altitude locations as well as at sea level.

Test Location

High altitude tests would be conducted at Denver, Colorado, which has an elevation of 5280 feet. A public road, which was used for the 1977 program, would be used for running the vehicle tests, and General Motors Emissions Test Facility would be used as the base of operations.

The low altitude tests would be run in the Los Angeles, California, area (200 feet altitude), and Union Oil Company Research Laboratories would be used as the base of operations for this portion of the program.

Reference Fuels

Octane requirements at all altitudes will be measured using the FBRU and FBRSU series of 1981 CRC unleaded full-boiling range fuels. Each fuel series will cover a range

of approximately 77 to 102 Research octane numbers and will be crossblended from three base fuels. Fuels for this program will be obtained from the same batch as those used in the 1981 CRC Octane Number Requirement Survey. Primary reference fuels will not be tested in this program, nor will ratings be determined on each vehicle's tank fuel.

Design specifications for octane number, lead content, and hydrocarbon type for each of the full-boiling range base fuels are shown in Table 1.

Cars

Eight models of 1981 cars have been selected, and ten cars of each model, except the GM cars with the 4.1L V-6 engine, will be rented in the Denver area. General Motors will provide six cars with the 4.1L V-6 engine for this program since none could be found in Denver car rental fleets. All of the cars will have accumulated at least 6,000 miles and will be in good mechanical condition. The following models have been selected:

| Make | Model | Engine DisplL | Type | Special Features |
|----------|---|------------------|------|------------------------|
| GM | Citation, Phoenix, Skylark, or Omega | 2.5 | L-4 | CLAF, EST |
| GM | Citation, Phoenix, Skylark, or Omega | 2.8 | V-6 | CLAF, EST |
| GM | Cutlass or Regal | 3.8 | V-6 | CLAF, EST, BARO |
| GM | Electra, 98, or Cadillac | 4.1 | V-6 | CLAF, EST, BARO |
| Ford | Mustang | 2.3 | L-4 | CLAF |
| Ford | Lincoln | 5.0 | V-8 | CLAF (F.I.), EST, BARO |
| Chrysler | Aries or Reliant | 2.2 | L-4 | CLAF, EST |
| Toyota | Corolla | 1.8 | L-4 | CLAF |

*Abbreviations: CLAF = closed loop air-fuel control

EST = electronic spark timing

BARO = spark advanced with decreasing

barometric pressure

Test Procedure

All tests will be conducted using the CRC E-15-81 test technique. Vehicle tests will be performed in the following sequence:

 Determine octane number requirements of all 76 cars at Denver (5280 feet). Cars which have octane requirements less than the lowest reference fuel will be rejected from the program, and additional cars with definable requirements will be tested as replacements. 2. Transport all 76 cars to Los Angeles, and determine octane number requirements at 200 feet elevation.

It is anticipated that eight to ten cars will be tested each day, thus the time required for on-site testing will be approximately two weeks in Denver and two weeks in Los Angeles. This allows a few extra days for preparation, bad weather, and scheduling problems.

Participation and Timing

Approximately 16 people will be needed to staff this program during the entire four-week period of testing at both locations. Minimum personnel requirements will be as follows:

5 rating crews (2 men each) = 10 total

2 mechanics

2 coordinators and data-handlers

2 fuel-handlers

The test program will begin in Denver on June 1, 1981.

LIMITING SPECIFICATIONS FOR 1981 FULL-BOILING RANGE REFERENCE FUELS*

| | Unleaded Average Sensit | ivity Reference | Puels (FBRU) | Unleaded High | Sensitivity Ref | Unleaded High Sensitivity Reference Fuel (FBRSU) |
|---|----------------------------|--------------------------------|--------------|---------------|-----------------|--|
| Inspection Tests | RMFD 332 RMFD 333 RMFD 334 | IMED 333 | RMFD 334 | RMFD 335 | NTD 336 | IMFD 337 |
| ASTM Distillation, °F(°C) | 90 (32.2) | 06 | 06 | 06 | 90 | 06 |
| 108 Evap. | 115-158 (46.1-70.0) | 115-158 | 115-158 | 115-158 | 115-158 | 115-158 |
| 30% Evap. | 150-190 (65.6-87.8) | 150-190 | 150-190 | 150-190 | 150-190 | 150-190 |
| 50% Evap. | 195-250 (90.6-121.1) | 195-250 | 195-250 | 195-250 | 195-250 | 195-250 |
| 708 Evap. | 230-300 (110.0-148.9) | 230-300 | 230-300 | 230-300 | 230-300 | 230-300 |
| 908 Evap. | 285-374 (140.6-190.0) | 285-374 | 285-374 | 285-374 | 285-374 | 285-374 |
| End Point, Max. | 437 (225) | 437 | 437 | 437 | 437 | 437 |
| KVP, psi (KPa) | 7-9 (48-62) | 7-9 | 7-9 | 7-9 | 7-9 | 7-9 |
| Lead, 9/gal (9/1) | <0.03 (<0.008) | <0.03 | <0.03 | <0.03 | <0.03 | <0.03 |
| Oxidation Stability, | | | | | | |
| minutes, minimum | 1440 | 1440 | 1440 | 1440 | 1440 | 1440 |
| Hydrocarbon Type, Vol & Arcmatics** Olefins Saturates | To be determined by ins | ned by inspection and reported | orted | | | |
| Octane Mumber Research | 7711 | 90±1 | 101±1 | 771 | 9011 | 10111 |
| Sensitivity*** | 41.5 | 7.71.5 | 111.5 | 6.0t.5 | 9.11.5 | 131.5 |
| Color | Clear | Green | Red | Yellow | Deep Purple | Light Blue |

All fuels to contain minimum 5 PTB of a 100% active anticxidant. No manganese added.

* To be compounded from normal refinery components ** 1% maximum Benzene or legal *** Sensitivites are shown for the mean Research Octane Number.

Minimum of two units sensitivity difference between corresponding fuels of each series.

Attachment 1

TECHNIQUE FOR DETERMINATION
OF OCTANE NUMBER REQUIREMENTS
OF LIGHT-DUTY VEHICLES

(CRC Designation E-15-81)

Revised

September 1980

TECHNIQUE FOR DETERMINATION OF OCTANE NUMBER REQUIREMENTS OF LIGHT-DUTY VEHICLES

(CRC Designation E-15-81)

A. GENERAL

The technique provides for the determination of octane number requirements of a vehicle in terms of borderline spark knock and surface ignition knock, regardless of throttle position, on two series of full-boiling range reference fuels as well as on primary reference fuels. It also provides octane requirements throughout the speed range on primary reference fuels.

Spark knock, surface ignition, and after-run characteristics of tank fuel will also be determined.

B. DEFINITION OF TERMS

- 1. The following definitions of knock were approved by the CFR and CLR Committees on June 8, 1954, and will be used in this technique. Knock is the noise associated with autoignition* of a portion of the fuel-air mixture ahead of the advancing flame front. The flame front is presupposed to be moving at normal velocity. With this definition, the source of the normal flame front is immaterial; it may be the result of surface ignition or spark ignition.
 - a. Spark Knock: A knock which is recurrent and repeatable in terms of audibility. It is controllable by the spark advance; advancing the spark increases the knock intensity, and retarding the spark reduces the intensity. This definition does not include surface ignition knock.
 - b. Surface Ignition Knock: Knock which has been preceded by a surface ignition. It is not controllable by spark advance.** It may or may not be recurrent and repeatable.

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^{*} Autoignition: The spontaneous ignition and the resulting very rapid reaction of a portion or all of the fuel-air mixture. The flame speed is many, many times greater than that which follows normal spark ignition. There is no time reference for autoignition.

^{**} For the purpose of this program, it is not intended that surface ignition knock be identified by manipulation of the spark advance.

- 2. The following definitions of knock intensity were specifically adopted for use in this technique:
 - a. No Knock: This means no spark knock or surface ignition knock.
 - b. Borderline Knock: This means spark knock of lowest audible intensity, recurrent surface ignition knock of borderline intensity, or infrequent (three or less) surface ignition knocks regardless of intensity.
 - c. Above Borderline Knock: This means greater than borderline spark knock, recurrent suface ignition knock greater than borderline intensity, or frequent (four or more) surface ignition knocks regardless of intensity.
 - d. After-Run: The engine continues to operate after the ignition is turned off.

3. Definition of Accelerations

Accelerations are made at maximum-throttle and partthrottle conditions which are defined below:

- a. Maximum-Throttle: The throttle is depressed and held at detent throughout the acceleration. This could be in highest gear or passing gear for automatic transmissions. The detent manifold vacuum obtainable on a given model is determined by the transmission characteristics.
- b. Part-Throttle: The throttle is depressed and regulated throughout the acceleration to maintain a desired, constant critical manifold vacuum in highest gear. Part-throttle will constitute any throttle position above detent vacuum up to the highest road load vacuum,
- c. 50th Percentile: The throttle is depressed and regulated to maintain an acceleration profile representative of average customer driving patterns.

C. VEHICLE PREPARATION

The following vehicle preparation steps should be completed before any octane tests are run. Detailed procedures for each adjustment can be found in the manufacturers' shop manuals.

1. Record vehicle identification number and emission control type, Federal, Altitude, or California. Fill in heading on data sheet DFMF-11-1181. Ford emission calibration numbers are to be recorded.

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- 2. Inspect all vacuum lines and air pump hoses for appropriate connections. Also, check to see if PCV valve, distributor vacuum delay valve, EGR valve, and heated inlet air mechanism are functioning. Engine must be warmed up for these checks.
- 3. Record engine idle speed and observe anti-dieseling solenoid operation. Adjust to manufacturers' recommended specifications as specified on the under-hood decal.
- 4. Observe and record basic spark timing at recommended engine speed. Adjust to manufacturers' recommended setting as specified on the under-hood decal.
- Crankcase oil, radiator coolant, automatic transmission fluid, and battery fluid levels shall be maintained as recommended by the manufacturer.
- 6. A calibrated tachometer graduated in 100 rpm (or smaller) increments and capable of indicating engine speed from 0-5000 rpm shall be installed on each vehicle.
- 7. One calibrated vacuum gage, graduated in one-half inch of mercury (or smaller) increments and capable of indicating vacuum from 0-24 inches of mercury (0-81 KPa) shall be connected to the intake manifold.
- 8. An auxiliary fuel system shall be provided to supply test fuels to the engine. Caution shall be taken to avoid placing auxiliary fuel lines in locations which promote vapor lock. If vehicles with carbureted engines have tank return fuel lines, this return line should be blocked off. Disconnect fuel tank vent line at evaporation control system canister. Instructions for fuel handling with fuel injection systems are given in Appendix A.
- 9. For vehicles equipped with knock sensor systems, instrumentation should be installed as described in Appendix B.
- 10. For vehicles with owner questionnaire completed, a sample of the tank gasoline shall be withdrawn for determination of Research and Motor method octane number ratings.

D. TEST PROCEDURE

1. Engine Warm-Up

- a. To stabilize engine temperatures, a minimum of ten miles of warm-up is required. The test vehicle should be operated at 55 mph (88 kph) in top gear with a minimum of full-throttle operation.
- b. During the warm-up period, the general mechanical condition of the vehicle should be checked to insure satisfactory and safe operation during test work.

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2. Fuel Change-Over

<u>Caution</u>: Because of the installation of catalytic devices on these vehicles, permanent damage may result if the engine runs lean or stalls. Therefore, change-over from one fuel to another must be accomplished without running the carburetor or fuel injection system dry. Fuel handling procedures for vehicles equipped with fuel injection systems are explained in Appendix A.

To eliminate contamination of the new fuel with residual amounts of the previous fuel, flush system twice with new fuel.

After fuel change-over, make one maximum-throttle acceleration before beginning Vehicle Rating Procedure.

3. Details of Observations

a. Operating Conditions

All octane number requirements will be determined under level road acceleration conditions.

Manual Transmissions: Vehicles with 3- and 4-speed transmissions shall be rated in highest gear. Vehicles with 5-speed transmissions shall be rated in 4th gear.

Automatic Transmissions: Automatic transmissions shall be run in the highest gear possible.

Tests will be conducted on moderately dry days, preferably at ambient temperatures above $60^{\circ}F$ (15.5° C). Tests should not be conducted during periods of high humidity such as prevail when rain is threatening or during or immediately after a rain storm. Laboratories with control capabilities should target for $70^{\circ}F$ (21°C) air temperature and 50 grains of water per pound (7.14 gm/kg) of dry air whenever possible.

Air-conditioned vehicles will be tested with air conditioner turned ON. (Normal setting, low fan)

b. Order of Fuel Testing

1. Tank

3. FBRU

2. FBRSU

4. Primary

c. Determination of Knock Intensity

Octane requirements will be established by evaluating the occurrence of knock in terms of knock intensity:

"N" for none, "B" for borderline, and "A" for above borderline. Establishment of representative knock intensity for a given fuel will be accomplished with the fewest number of accelerations possible. As defined below, the first two duplicating accelerations are sufficient with "N" and "B" knock intensity.

| Number | of Accele | rations | Representative | Rating |
|----------|-----------|---------|----------------|--------|
| <u>1</u> | 2 | 3 | | |
| N | N | - | N | |
| N | В | N | N | |
| N | В | В | В | |
| В | N | В | В | |
| В | В | - | В | |
| В | A | - | A | |
| Α | - | - | A | |

All subsequent accelerations will normally be discontinued when "A" knock intensity is experienced, and testing continued with a higher octane number fuel in that series. An exception will be made if "A" knock is experienced on the highest octane fuel which knocks in the engine. In this case, it may be necessary to run additional accelerations to determine the speed of maximum knock intensity. If "A" knock is experienced at initiation of acceleration, as limited by transmission characteristics, this speed will be considered the speed of maximum knock. Otherwise, the midpoint between knock-in and knock-out will be considered the speed of maximum knock. When establishing knock-in and knock-out, back off on the throttle between points to eliminate "A" knock. Tip-in knock should be ignored.

d. <u>Determination of Octane Requirements and After-Run</u> <u>Characteristics</u>

Tests should be run to 60 mph (97 kph) unless required to terminate at 55 mph (88 kph) because of legal speed limits.

The procedure for knock sensor equipped-cars is shown in Appendix B.

1) Vehicle Operating Procedure (for driver)

And the second second

a) For establishment of transmission characteristics, obtain top gear downshift engine rpm and manifold vacuum at 25, 35, 45, and 55 mph (40, 56, 72, 88 kph) by movement of the throttle through the detent position. Record both engine rpm and manifold vacuum at the downshift point for each speed.

The vehicle brakes may be applied lightly, if necessary, to maintain vehicle speed. In addition, for transmissions with converter clutches, determine the minimum vacuum and minimum road speed for converter clutch application. Record on data sheet.

- b) For maximum-throttle requirements in highest gear, accelerate at the detent position from the minimum obtainable speed as determined in (a)* up to 60 mph (97 mph). If transmission downshifts, abort and start acceleration again.
- c) For maximum-throttle requirements in passing gear for vehicles with automatic transmissions, accelerate from 10 mph (16 kph) below the starting speed for highest gear acceleration up to 60 mph (97 kph). When available, set shift gear selector to passing gear.
- d) For those vehicles with vacuum delay devices, to stabilize vacuum advance before starting each part-throttle acceleration, operate at road load for 40 seconds at the speed from which the acceleration is to begin.
- For part-throttle requirements, accelerate in highest gear at constant critical manifold vacuum from minimum obtainable speed to 60 mph (97 kph), or until vehicle ceases to accelerate. To obtain critical part-throttle vacuum, operate at road load for 40 seconds at 25, 35, 45, and 55 mph (40, 56, 72, and 88 kph). At each speed, move the throttle (in 3 to 5 seconds) from the highest road load vacuum down to detent manifold vacuum, or 1 inch Hg (3.4 KPa) above the minimum vacuum at which converter clutch engages. In this range, find a manifold vacuum for maximum knock intensity to use as the critical vacuum for all subsequent partthrottle accelerations. The vehicle brakes may be applied lightly, if necessary, to maintain vehicle speed, except for vehicles with converter clutch transmissions.

^{*} Starting speed for accelerations on manual transmission vehicles should be the lowest speed from which the vehicle will accelerate smoothly.

f) For 50th percentile requirements, follow the driving cycle described in Modes 1 and 2 below:

Mode 1: Idle 20 seconds. Make a 50th percentile acceleration through the gears to 60 mph. Decelerate to 55 mph and cruise for 0.5 mile. Decelerate moderately to 30 mph.

Mode 2: Cruise at 30 mph for 0.2 mile. Make a 50th percentile acceleration to 60 mph. Decelerate to 55 mph and cruise for 0.5 mile. Decelerate moderately to a stop.

Run the number of cycles necessary to be consistent with the table on page 15. Complete cycles (both modes) should be performed regardless of the mode in which knock occurs.

The 50th percentile acceleration profile is shown in Appendix C.

g) Determination of After-Run Characteristics

Determination of the occurrence of after-run will be evaluated on tank fuel. Following the engine warm-up, moderately brake the vehicle to a stop (foot off throttle) and place automatic transmission vehicles in park position, manual transmission vehicles in neutral. Air conditioner must be turned off. Immediately turn key to the "OFF" position. Note on the data sheet if after-run occurs.

2) Vehicle Rating Procedure (for rater)

Knock rating should be performed while in a normal seated position (head above instrument panel) with floor mats in place.

- Step 1 Using a fuel estimated to give borderline knock in a given fuel series, investigate for incidence of knock under conditions as described in 3d(1)(b) above, and 3d(1)(c) above.
- Step 2 If no knock occurs, go to a lower octane number blend in that series and repeat Step 1.

- Step 3 If knock occurs at one or more of the operating conditions in Step 1, continue investigation at the critical condition(s) with higher octane blends until highest octane fuel giving knock is determined within one octane number or one blend. Record maximum knock intensity on all fuels and speed of maximum knock intensity on highest octane fuel that knocks.
- Step 4 Using the lowest octane blend that did not knock in Step 3, investigate for incidence of part-throttle knock as described in 3d (1)(e). If knock occurs, continue investigation at critical vacuum until requirement is defined. Record maximum knock intensity and critical manifold vacuum on all fuels, and speed of maximum knock intensity on highest octane fuel that knocks.
- Step 5 With FBRU fuel only, investigate for incidence of knock with 50th percentile accelerations as described in 3d(l)(f). If knock occurs, continue investigation using both modes with higher octane blends until highest octane fuel giving knock is determined within one octane number or one blend. If no knock occurs, investigate for knock with lower octane number fuels until the requirement is determined or the lowest octane number fuel has been used. Record maximum knock intensity on all fuels, and mode, manifold vacuum, and speed of maximum knock intensity on highest octane fuel that knocks.

The rating procedure is given in arrow diagram form on page 21.

e. Tank Fuel Observations on Vehicles with Owner's Questionnaire

Investigate for maximum-throttle and part-throttle knock as detailed in Item 3d(1). Define maximum knock intensity as per Item 3c. Record maximum knock intensity, speed of maximum knock intensity, and manifold vacuum at each operating condition. Determine after-run characteristics as described in Item 3d(1)(g).

f. Octane Number Requirement Over Speed Range

Octane requirements over the speed range will be obtained on primary reference fuels only using throttle position

for maximum requirements. These will be established by recording the knock-in and knock-out points during maximum requirement acceleration with each incremental fuel investigated. It may be necessary to test one or two additional lower octane fuels to describe the knocking characteristics over the speed range. Accelerate at maximum-throttle from minimum obtainable speed as determined in 3d(1)(a), up to 3500 rpm, if necessary, in order to define requirements. These should be run to 60 mph (97 kph) unless required to terminate at 55 mph (88 kph) because of legal speed limits. If 3500 rpm cannot be attained in top gear, accelerations shall be discontinued and resumed in the next highest gear from 500 rpm below the engine speed at which top gear accelerations were determined.

When "A" knock is experienced, continue the acceleration, but back off on the throttle to maintain "B" knock until just prior to the knock-out point.

E. INTERPRETATION OF DATA

The data will be recorded on data sheet DFMF-11-1181. Octane requirements for all reference fuels shall be determined as follows:

- 1. If the knock intensity of the highest fuel giving knock is borderline, the requirement shall be reported as the octane number of that fuel.
- If the knock intensity of the highest fuel giving knock is above borderline, the requirement shall be reported as one-half the difference between the fuel giving knock and the next highest fuel.

Speed range data shall be reported on data sheet DFMF-11-1181 as the engine speed of knock-in and knock-out for the octane number of the primary reference fuel tested.

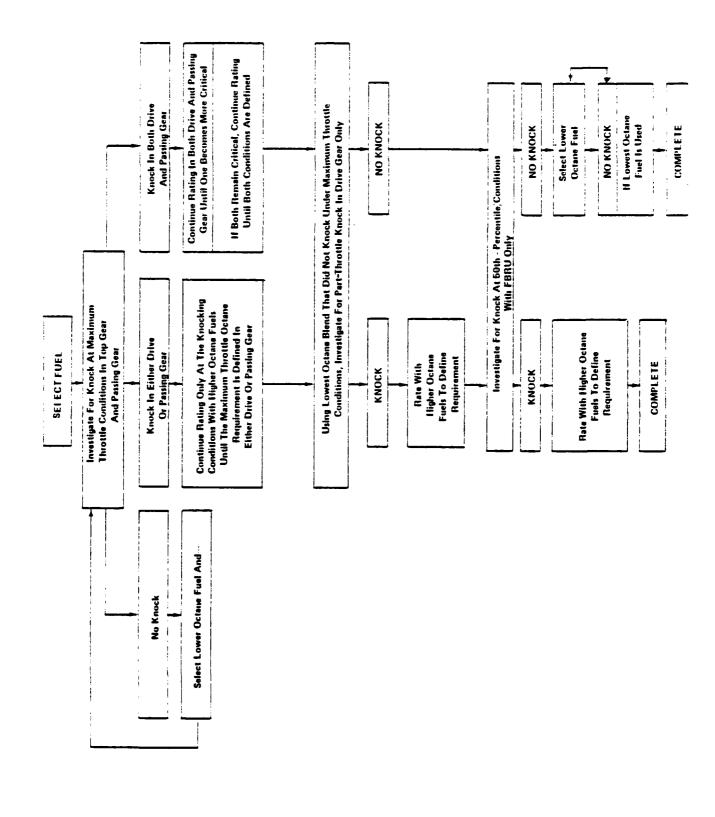
When transferring data to the summary report form, record "no" data as well as "yes" data.

Record data on all fuels tested, even though knock was not encountered. When transferring data to the summary report form DFMF-15-1181, record the higher among requirements under part-throttle and maximum-throttle condition for all fuels, and the 50th percentile requirement for FBRU fuel. Use proper letter designation (see footnotes on summary sheet) to designate requirements outside of the reference fuel limits.

Requirements for the various engine speeds will be determined by fitting a smooth curve through the knock-in and knock-out points

on work form DFMF-12-1181. Primary reference fuel requirements at various engine speeds should be reported to the nearest one-half octane number and recorded on the speed range summary sheets DFMF-25-1181.

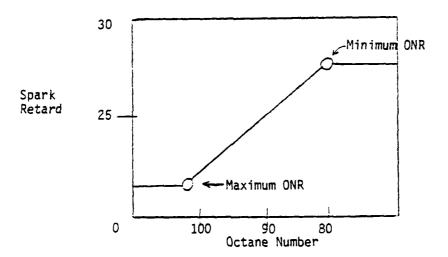
It is important that the vehicle identification number (VIN) of each vehicle tested be recorded on all data and summary sheets to provide a means of cross-indexing.



ONR MEASUREMENT WITH KNOCK SENSOR EQUIPPED VEHICLES - INSTRUMENT METHOD

The test method will define the limits of the vehicles ability to adapt to varying fuel quality. This will be accomplished by observing the knock sensor output as a function of spark retard. Also, the fuel quality for borderline knock will be determined.

Prepare the vehicle according to Section C (Vehicle Preparation) and, in addition, install a spark retard indicator. Using an estimated non-knocking fuel, accelerate as defined in B-3 and observe spark retard. Using lower octane fuels, continue testing until the maximum octane requirement and minimum octane requirement have been determined. The maximum requirement is the fuel quality at which spark retard begins. The minimum requirement is the fuel quality at which the spark retard reaches a maximum. (See Figure)



Record knock intensity on all fuels for maximum and minimum octane in accordance with B-2. Also, determine the octane number of the fuel that gives borderline knock using the accelerations defined in B-3. Record the degrees of spark retard associated with the borderline knock.

Data should be recorded on data form DFMF-26-1181 and plotted on curve sheet DFMF-27-1181.

APPENDIX D

DATA ON 1981 FULL-BOILING RANGE REFERENCE FUELS

TABLE D-I

OCTANE NUMBERS AND COMPOSITIONS FOR 1981 FBRU FUELS

| | | Volume | Percent | | | |
|-----|-----------|--------|---------|---------------|------|----------------|
| RON | RM 332 | | | FD -81 MON | SEN | <u>(R+M)/2</u> |
| 78 | 97 | .0 | 3.0 | - 74.3 | 3.7 | 76.2 |
| 80 | 82 | .5 1 | 7.5 | - 76.1 | 3.9 | 78.1 |
| 82 | 67 | .0 3 | 3.0 | - 77.8 | 4.2 | 79.9 |
| 84 | 52 | .0 4 | 8.0 | - 79.2 | 4.8 | 81.6 |
| 85 | 44 | .0 5 | 6.0 | - 79.8 | 5.2 | 82.4 |
| 86 | 36 | .0 6 | 4.0 | - 80.4 | 5.6 | 83.2 |
| 87 | 28 | .0 7 | 2.0 | - 81.0 | 6.0 | 84.0 |
| 88 | 20 | .0 8 | 0.0 | - 81.6 | 6.4 | 84.8 |
| 89 | 12 | .0 8 | 8.0 | - 82.1 | 6.9 | 85.6 |
| 90 | 4 | .0 9 | 6.0 | - 82.7 | 7.3 | 86.4 |
| 91 | | - 9 | 5.0 5 | .0 83.2 | 7.8 | 87.1 |
| 92 | | - 8 | 5.0 15 | 83.7 | 8.3 | 87.9 |
| 93 | | - 7 | 5.0 25 | .0 84.3 | 8.7 | 88.7 |
| 94 | | - 6 | 5.0 35 | .0 84.9 | 9.1 | 89.5 |
| 95 | | - 5 | 5.0 45 | .0 85.5 | 9.5 | 90.3 |
| 96 | | - 4 | 5.0 55 | 86.0 | 10.0 | 91.0 |
| 97 | | - 3 | 4.0 66 | .0 86.7 | 10.3 | 91.9 |
| 98 | | - 2 | 4.0 76 | 87.4 | 10.6 | 92.7 |
| 99 | • | - 1 | 5.0 85 | .0 88.1 | 10.9 | 93.6 |
| 100 | | - | 3.0 97 | .0 88.8 | 11,2 | 94.4 |

TABLE D-II

OCTANE NUMBERS AND COMPOSITIONS FOR 1981 FBRSU FUELS

| | | Volume Perce | nt | | | |
|-----|----------------|----------------|----------------|------|------|---------|
| RON | RMFD 335-81 | RMFD 336-81 | RMFD 337-81 | MON | SEN | (R+M)/2 |
| 78 | 96.0 | 4.0 | - | 72.2 | 5.8 | 75.1 |
| 80 | 81.0 | 19.0 | - | 73.6 | 6.4 | 76.8 |
| 82 | 65.0 | 34.0 | - | 75.1 | 6.9 | 78.6 |
| 84 | 51.0 | 49.0 | - | 76.5 | 7.5 | 80.3 |
| 85 | 43.0 | 57.0 | - | 77.3 | 7.7 | 81.2 |
| 86 | 35.5 | 64.5 | - | 78.0 | 8.0 | 82.0 |
| 87 | 27.5 | 72.5 | - | 78.7 | 8.3 | 82.9 |
| 88 | 20.0 | 80.0 | - | 79.4 | 8.6 | 83.7 |
| 89 | 12.0 | 88.0 | - | 80.1 | 8.9 | 84.6 |
| 90 | 4.0 | 96.0 | - | 80.8 | 9.2 | 85.4 |
| 91 | - | 96.0 | 4.0 | 81.4 | 9.6 | 86.2 |
| 92 | - | 87.5 | 12.5 | 82.1 | 9.9 | 87.1 |
| 93 | - | 79.0 | 21.0 | 82.8 | 10.2 | 87.9 |
| 94 | - | 70.0 | 30.0 | 83.4 | 10.6 | 88.7 |
| 95 | - | 61.0 | 39.0 | 84.1 | 10.9 | 89.6 |
| 96 | - | 52.0 | 48.0 | 84.8 | 11.2 | 90.4 |
| 97 | - | 42.5 | 57.5 | 85,5 | 11.5 | 91.3 |
| 98 | - | 33.0 | 67.0 | 86.2 | 11.8 | 92.1 |
| 99 | - | 22.5 | 77.5 | 86.9 | 12.1 | 93.0 |
| 100 | - | 10.0 | 90.0 | 87.6 | 12.4 | 93.8 |
| 101 | - | - | 100.0 | 88.3 | 12,7 | 94.7 |

TABLE D-III

INSPECTION DATA ON 1981 RMFD FUELS

| | | | Value for | RMFD Fuel | | |
|---|--|--|--|---|--|---|
| Property | 332 | 333 | 334 | 335 | 336 | 337 |
| ASTM Distillation | | | | | | |
| IBP (°F) 10% 30% 50% 70% 90% EP | 97 130 160 197 235 308 383 | 97 126 167 204 232 285 377 | 91 124 173 225 247 285 347 | 101 134 174 217 266 354 412 | 99 134 170 202 237 320 406 | 103 131 179 232 268 315 390 |
| API Gravity | 66.9 | 62.2 | 53.1 | 62.8 | 58.1 | 53.5 |
| RVP (psi) | 8.4 | 9.0 | 9.0 | 7.3 | 7.6 | 8.2 |
| Pb (g/gal) | <0.003 | <0.003 | <0.003 | <0.003 | <0.003 | <0.003 |
| Oxidation Stability (min) | >1440 | >1440 | >1440 | >1440 | >1440 | >1440 |
| Hydrocarbon Composition (Volume %) | | | | | | |
| Saturates (P+N) Olefins Aromatics | 77 5 18 | 74 8 18 | 53 0 47 | 51 33 16 | 65 10 25 | 52 5 43 |
| Research O.N. | 77.4 | 90.7 | 100.4 | 77.8 | 90.7 | 101.5 |
| Motor O.N. | 73.6 | 82.9 | 89.1 | 71.4 | 80.8 | 88.4 |
| Sensitivity | 3.8 | 7.8 | 11.3 | 6.4 | 9.9 | 13.1 |

TABLE D-IV

COMPOSITION DATA ON 1981 RMFD FUELS

| | | | /olume % i | n RMFD Fue | 1 | |
|-----------------------------------|------|------|------------|------------|------|------|
| Component | 332 | 333 | 334 | 335 | 336 | 337 |
| Mixed Xylenes | 5.5 | | 7.4 | | | 14.4 |
| Nonyl Aromatics | | 2.2 | 7.4 | | 3.9 | 14.3 |
| Heavy Platformate | | 8.4 | 34.6 | | 8.7 | 12.2 |
| Cyclopentane | | 4.8 | 6.7 | | 7.8 | 9.4 |
| ASTM Isooctane | 2.7 | | 14.8 | | | 19.8 |
| Soltrol 10 | 9.1 | 11.7 | | | 9.7 | |
| n-Butane | 3.4 | 5.6 | 5.0 | 2.5 | 3.9 | 4.4 |
| iso-Pentane | | 8.1 | 15.7 | | 4.9 | 13.3 |
| Cat Cracked Gasoline | 10.9 | | | 74.9 | | 12.2 |
| Housebrand Gasoline Base Blend | | 28.5 | | | 36.9 | |
| Soltrol 50 | | 11.7 | | | | |
| Cyclohexane | | 12.1 | | | 13.6 | |
| Refinery Platformate | 27.7 | 2.1 | | | 7.8 | |
| iso-Hexanes | 13.4 | | | | | |
| n-Pentane | 13.7 | 2.5 | 8.4 | 8.6 | | |
| n-Hexane | 4.0 | 2.3 | | | | |
| ASTM n-Heptane | 9.6 | | | 14.2 | 2.8 | |

APPENDIX E

WEATHER CONDITIONS FOR THE 1981 ALTITUDE

OCTANE REQUIREMENT PROGRAM

TABLE E-I

BAROMETRIC PRESSURE, In. Hg

| Group | Hi | ah | Ĺ | ow | Mea | an |
|------------|-------------|--------|-------|--------|-------|--------|
| No. | LA | Denver | LA | Denver | LA | Denver |
| | | | | | | |
| 1 | 29.70 | 24.78 | 29.64 | 24.63 | 29.67 | 24.71 |
| 2 | 29.72 | 24.80 | 29.42 | 24.53 | 29.57 | 24.66 |
| 3 | 29.70 | 24.80 | 29.59 | 24.73 | 29.64 | 24.76 |
| 4 | 29.70 | 24.80 | 29.61 | 24.53 | 29.66 | 24.67 |
| 5 | 29.71 | 24.80 | 29.59 | 24.60 | 29.65 | 24.70 |
| 6 | 29.73 | 24.70 | 29.61 | 24.55 | 29.67 | 24.62 |
| 7 | 29.73 | 24.78 | 29.60 | 24.53 | 29.67 | 24.66 |
| 8 | 29.71 | 24.68 | 29.67 | 24.55 | 29.69 | 24.62 |
| All Groups | 29.73 | 24.80 | 29.42 | 24.53 | 29.65 | 24.68 |

TABLE E-II

ABSOLUTE HUMIDITY

(Grains H₂0/lb Dry Air)

| Group No. | LA H | igh Denver | LA | _ow | <u>Me</u> | Denver |
|--------------|------|---------------|----|---------|-----------|--------|
| 1 | 82 | 96 | 56 | 52 | 69 | 74 |
| 2 | 92 | 91 | 50 | 59 | 71 | 75 |
| 3 | 85 | 82 | 26 | 66 | 56 | 74 |
| 4 | 85 | 96 | 26 | 59 | 56 | 78 |
| 5 | 86 | 96 | 36 | 65 | 61 | 81 |
| 6 | 85 | 84 | 70 | 68 | 78 | 76 |
| 7 | 85 | 89 | 66 | 59 | 76 | 74 |
| 8 | 92 | 83 | 64 | 60 | 78 | 72 |
| All Groups | 92 | 96 | 26 | 52 | 68 | 76 |

TABLE E-III

AMBIENT TEMPERATURE, °F

| Group | Н | ligh _ | Lo | ow | Me | an |
|------------|-----|--------|------------|--------|----|--------|
| No. | LA | Denver | LA | Denver | LA | Denver |
| | | | | | | |
| 1 | 104 | 79 | 6 8 | 72 | 86 | 76 |
| 2 | 104 | 95 | 77 | 76 | 91 | 86 |
| 3 | 110 | 84 | 80 | 68 | 95 | 76 |
| 4 | 107 | 95 | 77 | 73 | 92 | 84 |
| 5 | 110 | 83 | 75 | 68 | 92 | 76 |
| 6 | 93 | 87 | 80 | 69 | 86 | 78 |
| 7 | 93 | 95 | 72 | 69 | 82 | 82 |
| 8 | 95 | 91 | 73 | 69 | 84 | 80 |
| All Groups | 110 | 95 | 68 | 68 | 88 | 80 |

APPENDIX F

INDIVIDUAL CAR DATA

| TS | 1.0 | 8.0 | 2.0 | 0.5 | 0.5 | 0.0 | 2.0 | 2.0 | 0.0 | 1.5 | - |
|-------------------------------------|------------|---------|----------|-------------|---------|---------|----------|------------|----------|-----------|--------------------|
| REMENTS N G VAC | K D | K D | × | × | N O | × | Α D | × | Z D | K | GROUP 1) |
| HAX REQUIREMENTS T OCTANE N G VA | 87.5 | 91.0 | 93.0 | 87.0 | 87.0 | 87.5 | 91.0 | 0.96 | 92.0 | 87.0 | NVER |
| HAM | I | • | Σ | Σ | E | Σ | Σ | X | Σ | x | - DE |
| VAC M | 1.0 1 | 7.5 1 | 11.0 1 | 3.0 1 | 1.0 2 | 1.0 1 | 6.0 2 | 5.0 1 | 1.0 1 | 4.5 1 | (RAW DATA - DENVER |
| MPH | 40. | 28. | 20. | 35. | 51. | 48. | 35. | 40. | 45. | 45. | (RA |
| NU SO PERCENTILE * | 87.5 | 88.0 | 92.0 | 84.0 | 84.0 | 85.0 | 0.06 | 0.96 | 90.5 | 85.0 | |
| FBRU FEQUIREMENTS | K P 1.0 | K D 8.0 | К Р 2.0 | K P 0.5 | K D 0.5 | К Р 0.0 | K P 2.0 | K D 2.0 | КР 0.0 | K D 1.5 | |
| X REQUIE | 87.5 | 88.0 | 92.0 | 86.0 | 86.0 | 87.0 | 0.06 | 95.0 | 0.06 | 85.0 | |
| Y L | X | Δ. | × | X | Σ | Σ | Σ | Σ | Σ | Σ | |
| R GR/LB | 56. | 57. | .09 | 62. | 82. | .09 | .99 | .09 | 58. | 62. | |
| WEATHER BAROM GR/LB | 104. 29.67 | 29.64 | 29.65 | 29.64 | 29.70 | 29.62 | 29.68 | 29.69 | 29.68 | 90. 29.65 | |
| TEMP | 104. | 68. | 85. | .06 | 74. | 85. | 88 | 94. | 93. | .06 | |
| MILES | 8746 | 8680 | 11431 | 11300 | 7380 | 7855 | 10444 | 8100 | 6336 | 7940 | |
| COMP | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | |
| dSIG | 2.8 | 2.8 | 8.2 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | |
| SEN | z | z | z | Z | z | z | Z | Z | z | z | |
| VEHICLE MIS BBL | 2 | 7 | 7 | 2 | 7 | 2 | 2 | 7 | 2 | 7 | |
| VEH | įa. | (a. | <u> </u> | 52 - | ía. | Δ. | 6 | 54. | 5 | ia. | |
| HAN COLS CODE EMIS | 101 | 101 | LC7 | rc1 | 101 | 107 | LC7 | 107 | 101 | 101 | |
| 088 | 101 | 111 | 12L | 13L | 1 4 L | 151 | 16L | 171 | 181 | | |
| STAD | V-6 10L | V-6 11L | V-6 12L | V-6 13L | V-6 14L | V 6 15L | V-6 16L | V-6 17L | V-6 18L | N-6 19L | |

(RAW DATA - LOS ANGELES GROUP 1)

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

| | OCTANE MPH VAC M T OCTANE N G VAC | 50. 2.0 1 M 83.0 K P 2.0 | 45. 2.0 1 M 82.0 K P 2.0 | 30. 3.0 3 M 85.0 K D 2.0 | 45. 3.0 1 M 82.0 K D 0.0 | 55. 0.0 3 M 81.0 K D 0.0 | 35. 3.0 2 M 84.0 K P 2.0 | 36. 5.5 3 M 80.0 K D 1.5 | 40. 1.0 2 P 84.0 K D 4.0 | 32. 3.0 2 H 83.0 K D 1.0 | |
|---------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-------------------------|
| ~1 | ,0, | 78.0 | 80.0 | 85.0 | 78.0 | 78.0 | 79.0 | 78.0 | 84.0 | 79.0 | 0 |
| FBRU | T OCTANE N G VAC | 83.0 K P 2.0 | 81.0 K P 2.0 | 85.0 K D 2.0 | 80.0 K D 3.0 | 80.0 KP 0.0 | 83.0 KP 2.0 | 80.0 K D 1.5 | 82.0 K D 4.0 | 81.0 K D 2.0 | |
| MAX REO | | × | × | × | × | ¥ | Σ | E | ىم | x | ; |
| WEATHER | TEMP BAROM GR/LB | 78. 24.66 55. | 78. 24.66 55. | 79. 24.78 90. | 76. 24.66 53. | 72. 24.66 63. | 75. 24.63 96. | 76. 24.66 52. | 78. 24.66 91. | 76. 24.66 54. | 10 77 76 11 |
| | DISP COMP MILES | 2.8 8.5 8650 | 2.8 8.5 8575 | 2.8 8.5 11353 79. 24.78 | 2.8 8.5 11217 | 2.8 8.5 7311 | 2.8 8.5 7717 | 2.8 8.5 10313 | 2.8 8.5 7993 | 2.8 8.5 6214 | ** ** ** ** ** ** ** ** |
| VEHICLE | S BBL LEN | 2 N | 2 N | 2 8 | 2 N | 2 N | 2 % | 2 N | 2 N | 2 N | |
| V | CODE | 1C7 F | LC7 F | LC7 F | LC7 F | IC7 F | 1C7 F | LC7 F | 107 P | 1C7 F | , |
| | CYLS OBS | 1 0 D | V-6 11D | V-6 12D | V-6 13D | V-6 14D | V-6 150 | V-6 16D | V-6 17D | V-6 18D | |

* 50th Percentile Acceleration Technique

NOTE: G = GEAR. M = MODE. N = NOISE. T = THROTTLE POS.

| 1 14 12 12 13 | N G VAC | 92.0 K D 2.0 | 93.0 K D 2.0 | 95.0 K D 2.0 | K D 1.0 | K P 1.5 | K D 2.0 | K D 2.0 | K D 2.0 | K D 2.0 | 97.0 K D 5.5 |
|---------------------------|------------------------------|---------------------|---------------------|---------------------|-------------------------------|---------------------------|---------------------|---------------------|---------------------|-------------------------|----------------------------|
| FBRSU | T OCTANE N G VAC | 92.0 | 93.0 | 95.0 | 0.06 | 92.0 | 92.0 | 91.0 | 89.0 | 93.0 | |
|); | ¥ L | Z | 2.0 2 M | T | X | I | × | x | Σ | X | ۵, |
|]. | Σl | ~ | 7 | 2.0 1 M | - | 2.0 1 | 2.0 1 | 2.0 3 | 2.0.2 | 2.0 2 M | - |
| | VAC | 2.0 1 | | | 1.5 1 M | | | | | | 93.0 54. 2.0 1 P |
| | MPH | 47. | 50. | 92.0 50. | 35. | 91.0 50. | 45. | . 80 | 45. | 50. | 54. |
| FBRU | OCTANE MPH VAC M | 90.0 | 89.0 | 92.0 | 88.0 35. | 91.0 | 89.0 | 90.0 | 87.0 | 91.0 | 93.0 |
| E | VAC | 2.0 | 2.0 | 2.0 | 1.0 | 1.5 | 2.0 | K D 2.0 | 2.0 | 2.0 | 2.0 |
| 12 | | Α | K D | K D | M D | ¥ | K D | K D | K D | Z Y | Z D |
| 11 | T OCTANE N G VAC | 90.0 K D 2.0 | 91.0 K D 2.0 | 94.0 K D 2.0 | 88.0 K D 1.0 | 91.0 K P 1.5 | 90.0 K D 2.0 | 0.06 | 88.0 K D 2.0 | 91.0 K D 2.0 | 93.0 K D 2.0 |
| | X IOI | 6 | 5 | 55 | ٣ | 5 | 6 | 5 | Œ | 5 | |
| 1: | | I | I | Σ | Œ | Σ | X | Σ | I | X | ¥ |
| , | GR/LB | 72. | 67. | 72. | 17. | .09 | 50. | 82. | 76. | 92. | 56. |
| | | | | | | | | | | | |
| | BAROM | 29.42 | 29.62 | 29.71 | 29.72 | 29.69 | 29.63 | 29.68 | 29.67 | 29.66 | 19.62 |
| | TEMP BARON G | 77. 29.42 | 94. 29.62 | 89. 29.71 | 80. 29.72 | 94. 29.69 | 85. 29.63 | 91. 29.68 | 78. 29.67 | 84. 29.66 | 104. 29.61 |
| | TEMP | | | | 0365 80. 29.72 | 15205 94. 29.69 | | | 14770 78. 29.67 | 10305 84. 29.66 | 4051 104. 29.61 |
| | | | 8.0 11730 | 8.0 12088 | 8.0 10365 80. 29.72 | 8.0 15205 94. 29.69 | 8.0 11942 | 8.0 11430 | 8.0 14770 | 8.0 10305 | 8.0 14051 104. 29.61 |
| | | 3.8 8.0 11852 | | | 3.8 8.0 10365 80. 29.72 | 3.8 8.0 15205 94. 29.69 | | | | 3.8 8.0 10305 84. 29.66 | 3.8 8.0 14051 104. 29.61 |
| | | | 8.0 11730 | 8.0 12088 | N 3.8 8.0 10365 80. 29.72 | N 3.8 8.0 15205 94. 29.69 | 8.0 11942 | 8.0 11430 | 8.0 14770 | 8.0 10305 | N 3.8 8.0 14051 104. 29.61 |
| | BEL SEN DISP COMP HILES | 3.8 8.0 11852 | 8.0 11730 | 8.0 12088 | 2 N 3.8 8.0 10365 80. 29.72 | 3.8 | 8.0 11942 | 3.8 8.0 11430 | 8.0 14770 | 3.8 8.0 10305 | |
| | SEN DISP COMP HILES | 3.8 8.0 11852 | 8.0 11730 | 8.0 12088 | A 2 N 3.8 8.0 10365 80. 29.72 | 3.8 | 8.0 11942 | 3.8 8.0 11430 | 8.0 14770 | 3.8 8.0 10305 | |
| | BEL SEN DISP COMP HILES | 3.8 8.0 11852 | 2 N 3.8 8.0 11730 | 2 N 3.8 8.0 12088 | 2 N | 2 N 3.8 | 2 N 3.8 8.0 11942 | 2 N 3.8 8.0 11430 | 2 N 3.8 8.0 14770 | 2 N 3.8 8.0 10305 | 2 N |
| | EMIS BBL SEN DISP COMP MILES | A 2 N 3.8 8.0 11852 | A 2 N 3.8 8.0 11730 | A 2 N 3.8 8.0 12088 | A 2 N | A 2 N 3.8 | A 2 N 3.8 8.0 11942 | A 2 N 3.8 8.0 11430 | A 2 N 3.8 8.0 14770 | A 2 N 3.8 8.0 10305 | A 2 N |

| 1 10 | 21 | 2.0 | 0. | 0. | 0. | 0 | 0. | 0. | • | • | • |
|--|---------------------------------------|--------------|-------------------------|---------------------|---------------------|--------------|--------------|--------------|--------------|--------------|-------------------------|
| FINT | > 1 > 1 | K D 2 | K D 2.0 | K P 2.0 | K D 2.0 | K D 2.0 | K D 0.0 | K D 2.0 | K D 2.0 | K D 2.0 | D 2 |
| SUIRE | = 1 | | | ¥ | | × | | × | | | ¥ |
| FBRSU MAX REQUIREMENTS T OCTANE N C VAC | 21012 | 90.0 | 87.0 | 90.0 | 88.0 | 90.0 | 89.0 | 88.0 | 88.0 | 89.5 | 92.0 K D 2.0 |
| HA | 4 } | æ | Σ | ¥ | Σ | × | × | X | Œ | X | X |
| 50 PERCENTILE * | | 2.5 1 | 2.5 1 | 2.0 2 | 2.0 1 | 2.0 1 | 2.0 1 | 2.0 1 | 2.0 1 | 2.0 1 | 2.5 1 M |
| RCENT | | 35. | 45. | 35. | 45. | 50. | 33. | 45. | 45. | 45. | 91.0 45. |
| 1 19 | | 88.0 | 85.0 45. | 88.0 | 84.0 | 88.0 | 88.0 | 86.0 | 85.0 | 87.0 45. | 91.0 |
| FBRU HAX REQUIREMENTS T OCTANE N C VAC O | | 87.0 K D 0.0 | 85.0 K D 2.0 | 88.0 KP 2.0 | 87.0 K D 2.0 | 88.0 K D 2.0 | 88.0 K D 0.0 | 86.0 K D 2.0 | 86.0 K D 2.0 | 89.0 K D 3.0 | 91.5 K P 2.0 |
| REQUIR | | 87.0 | 85.0 | 88.0 | 87.0 | 88.0 | 88.0 | 86.0 | 86.0 | 89.0 | 91.5 |
| HAX | 5 i - 1 | E | × | ¥ | x | Σ | Œ | ¥ | Σ | æ | I |
| R Colle | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 68. | 82. | 89. | 91. | 80. | 82. | 59. | 63. | 59. | 82. |
| WEATHER TEMP RABOM COTTR | | 76. 24.70 | 3.8 8.0 11638 80. 24.70 | 8.0 11997 79. 24.78 | 8.0 10280 78. 24.80 | 95. 24.56 | 80. 24.76 | 91. 24.57 | 82. 24.53 | 91. 24.57 | 3.8 8.0 13950 80. 24.78 |
| N N | | 76. | 80. | 79. | 78. | | | 91. | | 91. | 80. |
| AND GOND MITER | 20071 | 8.0 11750 | 11638 | 11997 | 10280 | 8.0 15123 | 8.0 11880 | 8.0 11337 | 8.0 14673 | 8.0 10147 | 13950 |
| AMO. | | 8.0 | 8 0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| 9010 | 1010 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |
| 2 | 12 | z | z | z | z | z | 2 | z | z | z | æ |
| | | 7 | 7 | 2 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| VEHICLE | | < | < | <u>.</u> | < | < | < | < | < | < | < |
| 9000 | 2 | 114 | 114 | 114 | LIA | 114 | 114 | LIA | 114 | LIA | LIA |
| 0 0 0 | 2 | 20D | 210 | 22D | 230 | 24D | 25D | 26D | 27D | 28D | 29D |
| 3 | 3 | 9-1 | 9-A | V-6 22D | V-6 23D | V-6 24D | V-6 25D | V-6 26D | V-6 27D | V-6 28D | V-6 29D |

(RAW DATA - DENVER GROUP 2)

* 50th Percentile Acceleration Technique

NOTE: G = GEAR. M = MODE. N = NOISE. T = THROTTLE POS.

HAX REQUIREMENTS

T OCTANE N G VAC (RAW DATA - LOS ANGELES GROUP 3) 87.0 K P 0.0 K D 2.0 K P 0.0 K P 2.0 91.0 89.0 0.06 0.06 0.06 92.0 89.0 95.0 88.0 Σ Σ Σ Z. Σ SO PERCENTILE * 3.5 1 3.0 1 2.0 1 3.0 1 4.0 1 0.0 2 0.0 4.0 1 2.5 2 2.0 1 40. 34. 19. 25. 30. 25. 30. 30. 35. 45. OCTANE 0.46 85.0 88.0 85.0 89.0 88.0 0.06 88.0 88.5 FBRU MAX REQUIREMENTS

T OCTANE N G VAC K D 2.0 K D 0.0 K D 2.0 K P 0.0 K D 2.5 K D 2.0 K D 2.5 K D 2.0 K D 2.5 K D 2.0 1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES 87.0 86.0 89.0 88.0 89.0 89.0 0.06 88.0 0.76 89.0 I Σ X Σ I Σ Σ Σ Σ Σ WEATHER TEMP BAROM GR/LB 26. 62. 57. 46. 26. 50. 36. 86. 29.64 6415 92. 29.65 7510 107. 29.68 97. 29.63 95. 29.64 85. 29.63 6218 110. 29.59 7845 107. 29.68 98. 29.61 80. 29.70 6898 6241 7053 6335 0969 COMP MILES 9.0 6137 0.6 0.6 0.6 0.6 9.0 0.6 9.0 0.6 0.6 VEHICLE 1.8 1.8 1.8 1.8 1.8 8:1 CYLS OBS CODE EMIS 316 32L 331 4 34L 4 35r 4 361 4 37L 38L 4 30L 4 39L

| | REMENTS N C VAC | 2.0 | 0.0 | 1.5 | 0.2 | 2.0 | 2.0 | 1.0 | K D 2.0 | K D 2.0 | 2.0 |
|-------|--------------------------------------|--------------|--------------|-----------|----------------|--------------|-------------|--------------|-----------|----------------|----------------|
| 5 | NEW | | ™ | 7 0 | <u>a.</u> ≌ | <u>a.</u> | a. ≌ | 7 | 7 | × | × |
| FBRSU | HAX REQUIREMENTS T OCTANE N G VAC | 81.0 | 81.0 | 81.0 | 82.0 | 82.0 | 82.0 | 80.0 | 81.0 | 84.0 | 86.0 K D 2.0 |
| | Z L | , 1 = | X | I | x | × | I | ¥ | E | E | ¥ |
| | TILE * | 2.0 1 | 1.0.1 | 2.0 1 | 3.0 1 | 2.0 1 | 2.0 1 | 3.0 3 | 2.0 1 | 2.0 1 | 2.0 3 M |
| | RCEN | 28. | 35. | 22. | 25. | 30. | 25. | 12. | 25. | 28. | 20. |
| | SO PERCENTILE * | 78.0 | 78.0 | 79.0 | 80.0 | 80.0 | 80.0 | 78.0 | 80.0 | 80.0 | 84.0 |
| FBRU | REMENTS N G VAC | 79.0 K P 2.0 | 80.0 K D 0.0 | K D 1.5 | K P 2.0 | K D 2.0 | K P 2.0 | K D 1.0 | K P 2.0 | K D 2.0 | 84.0 K D 2.0 |
| | MAX REQUIREMENTS T OCTANE N G VA | 79.0 | 80.0 | 79.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 84.0 |
| | EIL | Σ | Σ | I | I | X | X | X | Œ | X | X |
| | GR/LB | 76. | 71. | 82. | 82. | 82. | .99 | .99 | 76. | 82. | 76. |
| | TEMP BARON GR/LB | 84. 24.73 | 77. 24.76 | 77. 24.76 | 77. 24.76 | 17. 24.76 | 68. 24.76 | 68. 24.76 | 84. 24.73 | 6894 77. 24.73 | 8625 74. 24.80 |
| | TEMP | 84. | | | 77. | 11. | 68. | 68. | | 11. | 74. |
| | SEN DISP COMP MILES | 6033 | 7388 | 6103 | 6962 | 6274 | 9469 | 6156 | 7715 | 6894 | |
| | COMP | 0.6 | 9.0 | 9.0 | 9.0 | 0.6 | 9.0 | 9.0 | 9.0 | 9.0 | 1.8 9.0 |
| | DISP | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 |
| | SEN | z | z | z | z | z | z | z | z | z | z |
| | CLE | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| | VEH | Sa. | (a. | ia. | <u> </u> | (34 , | 64 , | (a. , | ja, | (a. | ۵. |
| | CODE | - | - | ۲ | ۲ | ۲ | H | H | H | H | H |
| | 088 | 300 | 310 | 320 | 330 | 340 | 350 | 360 | 37D | 380 | 390 |
| | CYLS OBS | 47 | 4 | • | • | 4 | ₹ | -₹ | 4 | ₹ | 4 |

(RAW DATA - DENVER GROUP 3)

NOTE: G = GEAR. M = MODE. N = NOISE. T = THROTTLE POS.

^{* 50}th Percentile Acceleration Technique

(RAW DATA - LOS ANGELES GROUP 4) 1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

| | 1 101 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 0 |
|-------|---|----------------------------|-------------------------------|--------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---|
| | VA | - | | ö | 0 | 0 | 0 | | - | 2. | 0 |
| _ | NEW | × | Α 2 | K 2 | K 2 | Κ 2 | χ 2 | Ä | × | × 3 | K 2 |
| FBRSU | MAX REQUIREMENTS T OCTANE N G VAC | 94.0 K 3 1.0 | 96.0 K 2 0.0 | 96.0 K 2 0.0 | 96.0 K 2 0.0 | 97.0 K 2 0.5 | 92.0 K 2 0.0 | 94.0 K D 0.5 | 97.0 KP 1.0 | 96.0 K 3 2.0 | 94.0 K 2 0.0 |
| | X FI | Σ | 0.0 2 M | r | x | Σ | Σ | E | I | E | E |
| | ĮΣI | - | 7 | 7 | - | 1.0 1 M | 1.0 1 M | 1.0 1 M | 1.0 1 H | 2.0 1 M | - |
| | VAC | 0.0 | 0.0 | 0.0 | 0.0 | 0: | 1.0 | 1.0 | 1.0 | 2.0 | 0.0 |
| | HAX REQUIREMENTS 50 PERCENTILE * | 92.5 25. | 93.0 52. | 92.0 49. 0.0 2 M | 94.0 55. 0.0 1 M | 94.0 43. | 89.0 30. | 92.0 45. | 94.0 42. | 94.0 45. | 93.5 45. 0.0 1 M |
| | NE | 5. | 0.0 | 0. | 0: | 0. | 0.0 | 0: | 0: | 0 | 5.1 |
| RU | 5 1 1 1 1 1 1 | 92 | 6 | 92 | 76 | 76 | 80 | 92 | 76 | 76 | 93 |
| FBRU | N C | ٥. | 0 | 0 | 0 | • | ٥. | ٠. | 5 | 0. | ٥. |
| | GV | 3 1 | 2 0 | 2 0 | 2 0 | 2 0 | 3 0 | 0 0 | 0 0 | 4 2 | 3 0 |
| | I RE | × | × | × | × | × | × | × | × | ¥ | × |
| | ANE | 94.0 K 3 1.0 | 95.5 K 2 0.0 | 94.0 K 2 0.0 | 95.5 K 2 0.0 | 94.0 K 2 0.5 | 91.5 K 3 0.0 | 94.0 K D 0.5 | 94.5 K D 0.5 | 94.0 K 4 2.0 | 4.0 |
| | NX R | 6 | 6 | 6 | | | 6 | 6 | | | 6 |
| | 宝山 | Σ | X | X | X | I | Æ | Σ | Σ | I | Σ |
| | 1/LB | 83. | 34. | 70. | .09 | 85. M | 82. M | 78. | 83. | 50. | 26. |
| | ≃ [5] | | | | | | | | | | |
| | NTHER ROM GI | .61 | | . 70 | 89 | . 67 | 29 | . 70 | . 61 | 9 | 89 |
| | WEATHER BAROM GI | 29.61 | | 29.70 | 29.68 | 29.67 | 29.67 | 29.70 | 29.61 | 29.65 | 29.68 |
| | TEMP | 98. 29.61 | | 91. 29.70 | 94. 29.68 | 93. 29.67 | 80. 29.67 | 83. 29.70 | 98. 29.61 | 77. 29.65 | 107. 29.68 |
| | WEATHER LES TEMP BARON GI | 099 98. 29.61 | | 950 91. 29.70 | 179 94. 29.68 | 141 93. 29.67 | 673 80. 29.67 | 295 83. 29.70 | 168 98. 29.61 | 527 77. 29.65 | 651 107. 29.68 |
| | WEATHER MILES TEMP BARON GI | 9099 98. 29.61 | | 1 9950 91. 29.70 | 16179 94. 29.68 | 14141 93. 29.67 | 12673 80. 29.67 | 17295 83. 29.70 | 13168 98. 29.61 | 11527 77. 29.65 | 18651 107. 29.68 |
| | COMP MILES TEMP BARON GI | 8.4 9099 98. 29.61 | | 8.4 9950 91, 29.70 | 8.4 16179 94. 29.68 | 8.4 14141 93. 29.67 | 8.4 12673 80. 29.67 | 8.4 17295 83. 29.70 | 8.4 13168 98. 29.61 | 8.4 17527 77. 29.65 | 8.4 18651 107. 29.68 |
| | DISP COMP MILES TEMP BAROH GI | 5.0 8.4 9099 98. 29.61 83. | 5.0 8.4 17758 99, 29.62 | 5.0 8.4 9950 91, 29.70 | 5.0 8.4 16179 94. 29.68 | 5.0 8.4 14141 93. 29.67 | 5.0 8.4 12673 80. 29.67 | 5.0 8.4 17295 83. 29.70 | 5.0 8.4 13168 98. 29.61 | 5.0 8.4 17527 77. 29.65 | 5.0 8.4 18651 107. 29.68 26. Н 94.0 К 3 0.0 |
| | SEN DISP COMP MILES TEMP BAROH G | N 5.0 8.4 9099 98. 29.61 | | N 5.0 8.4 9950 91, 29.70 | N 5.0 8.4 16179 94. 29.68 | N 5.0 8.4 14141 93. 29.67 | N 5.0 8.4 12673 80, 29.67 | N 5.0 8.4 17295 83, 29.70 | N 5.0 8.4 13168 98, 29.61 | N 5.0 8.4 17527 77. 29.65 | N 5.0 8.4 18651 107. 29.68 |
| | CLE BBL SEN DISP COMP MILES | | 5.0 8.4 17758 99, 29.62 | | | | | | | | |
| | VEHICLE WEATHER EMIS BBL SEN DISP COMP MILES TEMP BAROH G | | 5.0 8.4 17758 99, 29.62 | | | | | | | | |
| | VEHICLE EMIS BBL SEN DISP COMP MILES | | 5.0 8.4 17758 99, 29.62 | | | | | | | | |
| | CLE BBL SEN DISP COMP MILES | Z L | F F N 5.0 8.4 17758 99, 29.62 | E L | E. | Z is. | Z L | Z G | Z L | Z L | 22 0a. 0a. |

(RAW DATA - DENVER GROUP 4)

| IRE | T OCTANE N G VAC | M 92.5 K D 3.0 | M 91.5 K D 1.0 | M 93.0 K D 2.0 | н 92.0 к D 0.0 | M 93.0 K D 0.0 | M 91.5 K D 0.0 | M 91.0 K D 0.0 | н 92.0 к D 0.0 | M 91.0 K D 0.5 | M 91.0 K D 1.5 | |
|-----------------------|------------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|-----------------------|----------------|----------------|------------------|
| 111E * | VAC | 0.0 2 | 0.0 | 0.03 | 0.01 | 2.5 1 | 0.0 1 | 2.0 1 | 0.5 1 | 2.5 1 | 2.0 2 | |
| RCEN | H d H | 35. | 30. | 33. | 35. | 34. | 20. | 45. | 49. | 28. | 50. | |
| 1 ! | OCTANE | 91.0 | 90.0 | 92.0 | 92.5 | 92.0 | 89.0 | 90.0 | 89.0 | 0.06 | 89.0 | |
| FBRU MAX REQUIREMENTS | N C VAC | K D 1.0 | K D 1.0 | K D 2.0 | K D 2.0 | K D 0.0 | K D 0.0 | K D 0.0 | K D 0.0 | K D 0.5 | K D 1.5 | |
| X REQUI | TOCTANE | 91.5 | 90.0 | 92.0 | 91.5 | 92.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | |
| | | × | X | × | Σ | × | I | ¥ | X | I | Σ | |
| 2 | GR/LB | 76. | 68. | 63. | 59. | 76. | 63. | 82. | 88. | 96 | 76. | |
| WEATHER | BAROM GR/LB | 24.78 | 76. 24.70 | 95. 24.56 | 24.57 | 24.76 | 82. 24.53 | 24.62 | 73. 24.66 | 75. 24.62 | 74. 24.80 | |
| 12 | TEMP | 74. | 76. | 95. | 91. | 84. | 82. | 78. | 73. | 75. | 74. | 2 |
| | MILES | 8988 | 17720 | 9848 | 16091 | 14083 | 12562 | 17243 | 8.4 13070 | 17458 | 8.4 18507 | T - THROTTLE POS |
| | COMP | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 4.8 | 8.4 | ⊨ |
| | DISP | 2.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | NOISE. |
| | SEN | Z | Z | Z | Z | Z | 2 | Z | Z | Z | z | NOI |
| VEHICLE | 887 | (a. , | 12. | 12. | ía, | <u> </u> | 124 | is. | ia. | (- | ia. | z |
| - (* | EMIS | ja. | 6 | D | Ca. | D ., | D. | P | L . | p. . | D. | . 30 |
| 1 | 2000 | M S | 3. | NS. | NS. | S | N K | NS. | AS | NS. | AS. | H = MODE. |
| | OBS | 400 | 4 1 D | 42D | 430 | 44D | 450 | 46D | 470 | 480 | 990 | |
| | CATS OBS CODE | V-8 40D | V-8 41D | V-8 42D | V-8 43D | V-8 44D | V-8 45D | V-8 46D | V-8 470 | V-8 48D | V-8 49D | NOTE: G - GEAR. |
| | | | | | | | | | | | | NOTE: G |

* 50th Percentile Acceleration Technique

FBRSU MAX REQUIREMENTS T OCTANE N G VAC K D 1.5 K M 0.0 K D 1.0 K P 2.0 K F 2.0 K P 1.5 K D 2.0 K D 2.0 K M 0.0 (RAW DATA - DENVER GROUP 5) 87.5 0.46 0.06 96.0 100.0 95.0 90.0 0.96 0.66 87.0 I Σ Σ X Σ ¥ ¥ Σ 2.0 1 50 PERCENTILE *
TANE MPH VAC H 3.0 1 30. . 2.0 1 2.0 1 0.0 4.0 1 2.0 1 3.0 1 3.0 1 0.0 45. 45. 40. 40. 30. 30. 35. 25. OCTANE 88.0 0.46 87.5 86.0 100.0 0.76 0.46 89.0 0.96 0.66 FBRU HAX REQUIREMENTS T OCTANE N G VAC K D 2.0 88.0 K D 1.5 94.0 K D 1.5 88.0 KM 0.0 K D 1.0 K P 2.0 K P 1.5 K P 0.0 94.0 87.0 98.0 M 100.0 89.0 0.96 93.0 Σ X Σ X X Σ Σ X Σ 84. 58. CLE BBL SEN DISP COMP HILES TEMP BAROH GR/LB .99 78. 83. 36. 70. 56. 46. 86. 75. 29.67 8.5 12330 106. 29.59 8.5 9450 110. 29.59 8.5 10470 83. 29.70 8.5 12730 92. 29.65 8.5 11840 85. 29.71 8.5 11128 104. 29.61 98. 29.61 8.5 10075 110. 29.59 8.5 13809 78. 29.70 8270 8.5 12192 8.5 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 VEHICLE EMIS BBL CYLS OBS CODE 51L 55L 56L 57L **58L** 4 50L 4 52L 4 53L 4 54L 4 59L

(RAW DATA - LOS ANGRLES GROUPS)

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

| | | | | | | | | | | | | | | FBRU | RU | | | | ,22, | FBRSU | | |
|--------------------|------|-------------|-------|----|------|------|---------------------|------|------------------|-------|----------|------------------|---------|---------|------------|-----------------|-------|---------|------------------|-------|----------|-----|
| | | VEHICLE | CLE | | } | | | | WEATHER | ~ | MAX | MAX REQUIREMENTS | REME | NTS | 50 PE | 50 PERCENTILE * | ILE * | 1 1 | MAX REQUIREMENTS | QUIR | EMEN | TS |
| CYLS OBS CODE EMIS | CODE | EM I S | 8 B L | EN | OISP | COMP | SEN DISP COMP MILES | TEMP | TEMP BAROM GR/LB | GR/LB | ól ⊢l | T OCTANE N G VAC | © ≥ | VAC | OCTANE MPH | H L | VAC | | T OCTANE N G VAC | NE I | ۱۵ اع | VAC |
| 4 500 | ¥ | 6 . | 7 | z | 2.2 | | 8.5 11892 | 68. | 68. 24.76 | 65. | ۵ | 91.0 | | K D 3.0 | 91.0 | 45. | 3.0 2 | | Н 91 | 91.0 | K D 2.0 | 2.0 |
| 4 51D | X | ja. | 7 | z | 2.2 | 8.5 | 8176 | 68. | 68. 24.76 | .99 | E | 81.0 | | K D 2.0 | 80.0 | 35. | 2.0 1 | | м 82 | 82.0 | K D 2.0 | 2.0 |
| 4 52D | X | Stee | 2 | 2: | 2.2 | | 8.5 12262 | 77. | 77. 24.76 | 71. | Œ | 81.0 K D 0.0 | × | 0.0 | 81.0 | 38. | 0.0 | | ¥8 # | 84.0 | к в 0.0 | 0.0 |
| 4 530 | ¥ | 6 | 7 | z | 2.2 | 8.5 | 9368 | 83. | 83. 24.60 | . 46 | I | 88.0 K D 1.5 | ¥ | 1.5 | 83.0 | 35. | 2.0 1 | | æ | 88.0 | K P 1.5 | 1.5 |
| 4 54D | ¥ | Da, | 7 | z | 2.2 | | 8.5 10357 | 75. | 75. 24.60 | 96. | Œ | 85.0 K D 2.0 | X | 2.0 | 84.0 | 45. | 2.0 | 2.0 3 M | | 86.0 | к р 2.0 | 2.0 |
| 4 550 | X | 1 | | z | 2.2 | 8.5 | 8.5 12634 | 79. | 79. 24.78 | 89. | X | 80.0 | Ā | K D 2.0 | 80.0 | 45. | 2.0 | 2.0 3 M | | 82.0 | K D 2.0 | 2.0 |
| 4 560 | ¥ | 12. | 7 | z | 2.2 | | 8.5 11775 | 78. | 78. 24.60 | 86. | Σ | 80.0 | | K D 2.0 | 80.0 | 25. | 2.0 1 | T. | | 84.0 | K D 2.0 | 2.0 |
| 4 57D | X | S L. | 7 | z | 2.2 | | 8.5 11051 | 77. | 77. 24.73 | 82. | ۵. | 82.0 K D 4.0 | Ä | 4.0 | 82.0 | 45. | 2.0 3 | | ж 82 | 82.0 | K D 2.0 | 2.0 |
| 4 580 | K | 2 | 7 | z | 2.2 | | 8.5 9959 | 75. | 75. 24.63 | 96. | I | 87.0 K D 1.5 | ¥ | 1.5 | 88.0 | 45. | 1.0 2 | 2 M | | 89.0 | K D 1.5 | 1.5 |
| 4 590 | X | 2 . | 2 | z | 2.2 | | 8.5 13680 74. 24.80 | 74. | 24.80 | 75. | I | 80.0 KP 1.0 | A P | 1.0 | 79.0 30. | 30. | 1.0 1 | ¥ | | 81.0 | K D 1.0 | 1.0 |

NOTE: G - GEAR. H - HODE. N - NOISE. T - THROTTLE POS.

* 50th Percentile Acceleration Technique

(RAW DATA - LOS ANGELES GROUP (1)

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

FBRSU HAX REQUIREMENTS T OCTANE N C VAC K D 1.0 K P 1.0 K D 2.5 K D 2.0 K D 0.0 K D 1.0 K P 0.0 K D 0.0 K D 0.0 K D 2.0 95.0 0.46 0.76 93.0 0.96 93.0 0.46 0.96 0.46 0.46 Σ Σ I Z Σ Σ X 0.0 2 TANE MPH VAC M 2.0 1 0.0 1.0.1 0.0 2.5 1 0.0 2.5 1 1.0 2 1.0.1 55. 50. 50. 55. 56. 54. 58. 55. 50. 50. OCTANE 94.5 93.0 93.0 0.06 95.0 92.0 92.0 94.0 95.0 95.0 FBRU HAX REQUIREMENTS T OCTANE N G VAC K D 0.0 K D 0.0 K D 2.0 K D 1.0 K D 2.5 K D 0.0 K D 0.0 K D 2.0 K D 1.0 K P 1.0 95.0 93.0 92.0 93.0 90.0 94.0 93.0 93.0 0.46 95.0 Σ Ľ X Σ Σ X Σ I I X, TEMP BAROH GR/LB 84. 77. .97 82. 85. 77. 84. 70. 74. 76. 29.68 29.61 29.69 29.68 29.64 86. 29.73 81. 29.67 29.67 80. 29.72 86. 29.73 91. 88. 93. 88. 86. 82. 9.0 11375 9.0 14639 SEN DISP COMP MILES 9.0 9235 9.0 15440 9.0 10243 9.0 10000 9.0 11125 9.0 12302 9.0 12701 9.0 11084 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 VEHICLE CYLS OBS CODE EMIS BBL MCA MCA ¥C. MCA MCA MCA MCA M CA MCA MCA 769 ¢ 4 61L \$ 62L 4 63L 799 P 4 65L 799 y 67L 189 4 60L

| | | | | | | | | | | | | | | | - | FBRU | | | | F.8 | FBRSU | | |
|-----------------|--------|-------|-----------|---------------------|-------------|--------|------|------|------------------|------|------------------------|-------|-----|-----------|------------------|------|-------|-------|--------------|------------------|----------|----------------|--|
| ÌΩΙ | CYLS 0 | 08S C | CODE | VERICLE EMIS BBL | | SEN | DISP | COMP | MILES | TEMP | WEATHER BAROM GR/LB | SR/LB | HAX | HAX REQUI | T OCTANE N G VAC | 181 | ERCEN | VAC | (= 1 | T OCTANE N G VAC | E N | MENTS G VAC | |
| | 4 | 4 009 | MCA | ₩. | 2 | 2 | 2.3 | 9.0 | 12613 | 80. | 24.70 | 82. | I | 84.0 | K P 2.0 | 84.0 | 35. | 2.0 | E | 85.0 | × | P 2.0 | |
| | 4 | 4 019 | MCA | • | 2 | z | 2.3 | 9.0 | 9113 | 87. | 24.55 | 72. | × | 83.0 | K D 1.0 | 84.0 | 45. | 1.0 | E ~ | 84.5 | × | D 1.0 | |
| | 4 620 | | H CA | • | 2 | z | 2.3 | 9.0 | 11080 | 76. | 76. 24.70 | . 89 | Œ | 85.0 | K D 1.0 | 85.0 | 54. | 1.0 3 | 3 | 87.0 | 0 × 0 | D 1.0 | |
| | 4 630 | | HCA | • | 2 | 2 | 2.3 | 0.6 | 11291 | 76. | 24.70 | 68. | × | 85.0 | K D 1.0 | 85.0 | 46. | 2.0 1 | Ξ | 87.0 | × | D 1.0 | |
| | 4 640 | | MCA | # | 7 | z | 2.3 | 9.0 | 15391 | 74. | 24.66 | 75. | X | 86.0 | K D 1.0 | 86.0 | 35. | 2.5 1 | π. | 88.0 | × | D 1.0 | |
| | 4 650 | | MCA | • | 7 | z | 2.3 | 9.0 | 10101 | 86. | 24.67 | 84. | Σ | 86.0 | K D 1.0 | 85.5 | 54. | 1.0 | | 88.5 | ₩ | P 0.0 | |
| | 4 660 | | MCA | ac) | 7 | z | 2.3 | 0.6 | 14535 | 74. | 24.66 | 75. | × | 82.0 | K P 2.0 | 84.0 | 25. | 3.0 1 | H | 84.0 | × | D 2.0 | |
| | 4 67D | | HCA | • | 8 | z | 2.3 | 9.0 | 9816 | 80. | 24.67 | 80. | Σ | 83.0 | K D 0.0 | 83.0 | 45. | 1.0 | 2 H | 85.0 | × | D 1.0 | |
| | 089 7 | | MCA | - | 7 | z | 2.3 | 9.0 | 9.0 12196 | 74. | 24.66 | 75. | × | 84.5 | K P 1.5 | 84.5 | 28. | 1.5 | ¥ ~ | 86.0 | × | P 1.5 | |
| | 969 ¥ | | MCA | • | 7 | z | 2.3 | 9.0 | 9.0 11011 | . 69 | 69. 24.68 | 68. | × | 83.0 | K D 0.0 | 83.0 | 48. | 0.0 | X | 83.0 | × | D 0.0 | |
| NOTE: G - CEAR. | AR. | r | H - MODE. | • | - 1 2 | NOISE. | | | T - THROTTLE POS | E P0 | | | | | | | | | | | | | |

(RAW DATA - DENVER GROUP ()

* 50th Percentile Acceleration Technique

| 5 | REQUIREMENTS CTANE N G VAC | K D 0.0 | K D 2.0 | K D 2.0 | K D 2.0 | K D 2.0 | K D 2.0 | K D 2.0 | K P 2.0 | K D 2.0 | K D 1.0 | GROUP 7) |
|-------|--------------------------------------|----------|-----------|---------|---------|----------|---------|---------------------|----------|----------|----------|----------------------|
| FBRSU | AX REQUI | 0.96 | 97.0 | 0.66 | 92.0 | 95.0 | 0.66 | 0.66 | 0.86 | 0.46 | 89.0 | (RAW DATA - DENVER (|
| | XI | Σ. | × | Σ | X | Σ | × | ¥ | X | ¥ | X | 0 - |
| | Į. | | 7 | - | - | - | - | | _ | - | - | Į. |
| | TILE * | | 2.0 | 3.0 | 4.0 | 4.0 | 3.5 1 | 3.0 | 7.0 | 4.0 1 | 1.0 1 | AW DA |
| | RCENT | 40. | 50. | 40. | 35. | 30. | 35. | .1 ¹ 25. | 15. | 25. | 36. | 3 |
| | SO PERCENTILE ** OCTANE MPH VAC | 91.0 | 94.0 | 0.66 | 92.0 | 95.0 | 98.0 | 0.66 | 98.0 | 94.0 | 86.0 | |
| FBRU | AC VAC | 0: | 2.0 | 0. | 0.2 | 0. | 0 | 0. | 2.0 | 2.0 | 1.0 | |
| | EN S | K D 0.0 | Ω | K D 2.0 | D 2.0 | D 2.0 | K D 2.0 | K D 2.0 | ۵ | 2 | K D 1 | |
| | N E | × | × | | ¥ | × | | × | × | × | ¥ | |
| | HAX REQUIREMENTS T OCTANE N G VAC | 92.0 | 94.0 | 99.0 | 91.0 | 94.0 | 99.0 | 99.0 | 98.0 | 94.0 | 87.0 | |
| | ¥ | Σ | X | ¥ | I | Σ | I | E | × | I | x | |
| | R GR/LB | 82. | 82. | 70. | .99 | 82. | 76. | 82. | .77. | 85. | 11. | |
| | WEATHER BAROH GR/LB | 29.60 | 72. 29.71 | 29.71 | 29.70 | 29.68 | 29.68 | 29.61 | 29.67 | 29.67 | 29.73 | |
| | TEMP | 91. | 72. | 89. | 91. | 91. | 8. | 91. | 81. | 93. | 86. | |
| | HILES | 6862 | 7000 | \$139 | 5750 | 7016 | 8279 | 6720 | \$665 | 6250 | 5300 | |
| | COMP | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | |
| | SEN DISP | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | |
| | | 2 | z | æ | 2 | 2 | z | z | z | z | z | |
| | CLE | ~ | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | |
| | VEHICLE EMIS BB' | - | # | • | • | # | æ | • | # | ~ | # | |
| | OBS CODE | 53 | rcs | rc s | rc s | rc s | LC 5 | rc3 | rcs | rc 2 | rcs | |
| | 385 | 701 | 71L | 72L | 7 3L | 74L | 75L | 797 \$ | 111 | 78L | 16L | |
| | CYLS | 4 | • | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | |

(RAW DATA - LOS ANGELES GROUP 7)

1981 CRC ALTITURE PROGRAM - 1981 VEHICLES

| n | MAX REQUIREMENTS | NCVAC | K D 0.0 | K D 1.0 | K D 5.0 | K D 2.0 | K D 2.0 | K P 2.0 | K D 2.0 | K D 2.0 | K D 2.0 | K D 2.0 |
|-------|------------------|---------------------|-----------|-------------|--------------|--------------|--------------|-----------|--------------|--------------|-----------|--------------|
| FBRSU | X REQUI | TOCTANE | 88.5 | 86.5 | 96.0 | 84.0 | 85.0 | 93.0 | 88.0 | 91.0 | 90.0 | 83.0 |
| | E | — 1 | x | Σ | ы | ¥ | X | X | Σ | E | I | E |
| | | Σl Oi | 0.0 | 1.0 1 | 3.0 1 | 2.0 3 | 2.0 3 M | 2.0 3 | 2.0 1 | 4.0 1 | 2.0 3 | 2.0 1 M |
| | 50 PERCENTILE * | VAC | | | | | | | | | | |
| | ERCEN | M M | 33. | 53. | 25. | 35. | 30. | 45. | 40. | 30. | 35. | 25. |
| FBRU | 1 1 | OCTANE MPI | 83.0 | 83.0 | 0.96 | 84.0 | 85.0 | 93.0 | 88.0 | 91.0 | 90.0 | 80.0 |
| 7.0 | S | 140 | 0.0 | 0:1 | 0.0 | 0. | • • | 0. | 0: | 0. | 0. | 0 |
| | EN. | 01 | K D 0.0 | <u>-</u> | 5 | 0 | 4 | K P 2.0 | 0 | 2 | K D 2.0 | 0 |
| | REP | Z! | × | × | × | × | × | × | × | × | × | × |
| | MAX REQUIREMENTS | OCTANE | 85.5 | 85.0 KP 1.0 | 96.0 K D 5.0 | 84.0 K D 2.0 | 84.0 K P 2.0 | 93.0 | 88.0 K D 2.0 | 90.0 K D 2.0 | 0.06 | 80.0 K D 2.0 |
| | ¥ | - 1 | X | ¥ | <u>α</u> , | X | × | X | ¥ | X | ¥ | X |
| | R | GR/LB | 89. | 59. | 63. | 59. | 69. | 68. | 68. | 84. | 63. | 63. |
| | WEATHER | TEMP BAROM GR/LB | 79. 24.78 | 91. 24.57 | 95. 24.56 | 91. 24.56 | 89. 24.57 | 69. 24.68 | 76. 24.70 | 86. 24.67 | 82. 24.53 | 82. 24.53 |
| | | | | | 95. | | | | | | | |
| | | SEN DISP COMP MILES | 6730 | 6870 | 5087 | 5687 | 6924 | 8117 | 6645 | 5904 | 6138 | 5241 |
| | | COMP | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 |
| | | DISP | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| | | S | 2 | × | z | × | 2 | 2 | 2 | × | × | 2 |
| | | 2 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| | VEH | EMIS | • | • | - | • | • | • | • | • | = | • |
| | | CODE | LCS | rc s | 105 | rcs | 105 | rc s | rc s | rcs | rcs | LCS |
| | | OBS | 7 O D | 710 | 72D | 7.30 | 74D | 7 S D | 76D | 7.7D | 78D | 19D |
| | | CYLS | • | • | • | • | • | • | • | • | • | 4 |

* 50th Percentile Acceleration Technique

NOTE: G - GEAR. M - MODE. N - NOISE. T - THROTTLE POS.

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

| FBRSU MAX REQUIREMENTS T OCTANE N G VAC P 94.0 K D 5.0 M 92.0 K P 1.0 P 94.0 K D 4.0 | FBRSU MAX REQUIREMENTS T OCTANE N G VAC M 82.0 K D 2.0 M 85.0 K D 2.0 M 86.0 K D 2.0 |
|---|---|
| FBRU MAX REQUIREMENTS 50 PERCENTILE * 1 OCTANE N G VAC OCTANE MPH VAC M P 94.0 K 3 5.0 91.5 35. 4.0 1 M 88.0 K D 1.0 88.0 50. 2.0 1 P 90.0 K D 4.0 88.0 50. 0.0 1 | FBRU |
| MEATHER TEMP BAROM GR/LB 84. 29.71 67. 95. 29.70 64. 92. 29.67 75. | MEATHER TEMP BAROM GR/LB 74. 24.66 75. 69. 24.68 69. 87. 24.55 72. 3TTLE. |
| VEHICLE CYLS 085 CODE EMIS BBL SEN DISP COMP MILES V-6 1L LR F 4 N 4.1 8.0 4500 V-6 2L GE F 4 N 4.1 8.0 6575 V-6 51 IR F 4 N 4.1 8.0 2368 | 2085 S |

* 50th Percentile Acceleration Technique

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

(RAW DATA - LOS ANGELES GROUP 8B)

| ام. | | VAC | 0.0.0 | 2.0 | 2.0 2.0 2.0 | | S | | VAC | 0.0.0 | 0.0.0 | 2.0 1.0 2.0 | i |
|--------------------|----------------|----------|----------------------|-----------------------|-----------------------|--------------------------|--------------------|----------------|----------|----------------------|------------------------|----------------------|-----------|
| MEN | Ę | | | | | | MENT | LE | | | | | |
| O I R | IROTI | 91 | ~~~ | | 000 | | UIRE | ROTT | 91 | | ~ ~ ~ | 444 | ĺ |
| REG | MAX THROTTLE | 21 | *** | *** | *** | | REQ | MAX THROTTLE | Zi | *** | *** | *** | |
| FBRSU REQUIREMENTS | M | OCTANE | 93.0 80.0 97.0 | 86.0 86.0 101.0 | 97.0 93.0 101.0 | (88) | FBRSU REQUIREMENTS | M. | OCTANE | 89.0 80.0 91.0 | 101.0 84.0 101.0 | 95.0 88.0 99.0 | |
| 1 | ļ | Σl | ~ e i | ∞ ∞ | 1 32 | ROUI | | | ΣÌ | ~ | ~ m ₁ | - 2 - | |
| | *3 | VAC | 2.0 | 2.0 2.0 2.0 | 2.0 | ER G | | * | VAC | 2.0 | 1.0 | 2.0 | |
| S | 50 PERCENTILE* | MPH | 50. 42. | 51. 48. 50. | 45. | DENV | S | 50 PERCENTILE* | MPH H | 45. | 45. 50. | 35. | |
| FBRU REQUIREMENTS | 50 PE | OCTANE | 92.0 80.0 93.0 | 98.0 85.0 100.0 | 98.0 96.0 100.0 | (RAW DATA - DENVER GROUP | FBRU REQUIREMENTS | 50 PE | OCTANE | 88.0 78.0 89.0 | 98.0 78.0 100.0 | 93.0 92.0 99.0 | |
| BRU RE | 3 | VAC | 0.0.0 | 2.0 2.0 2.0 | 2.0 2.0 2.0 | (RAI | BRU RE | 37 | VAC | 0.0.0 | 0.00 | 2.0 2.0 2.0 | |
| | 5 | 51 21 | *** *** | *** | ~ ~ ~ | | | <u>8</u> | ا2 ا | *** ••• | *** | ~ ~ ~ | |
| ļ | MAX THROTILE | | | | | | | MAX THROTTLE | | | | | |
| | Σ | OCTANE | 93.0 82.0 95.0 | 99.0 86.0 100.0 | 97.0 94.0 100.0 | | | Ì | OCTANE | 88.0 78.0 89.0 | 98.0 82.0 100.0 | 93.0 90.0 95.0 | |
| | PEO'T | TYPE | E-15 MIN MAX | E-15 MIN MAX | E-15 MIN MAX | | | 7,038 | TYPE | E-15 MIN MAX | E-15 MIN MAX | E-15 MIN MAX | |
| | | GR/LB | .69 | 92. | 70. | | | | GR/LB | .09 | 83. | 68. | |
| | WEATHER | BAROM | 29.70 | 29.67 | 29.69 | | | WEATHER | BAROM | 24.55 | 24.55 | 24.55 | |
| | | TEMP | 85. | 73. | 82. | | | į | TEMP | 91. | 96. | . 69 | |
| | | MILES | 7104 | 3570 | 4690 | | | | MILES | 6944 | 3390 | 4420 | |
| | | COMP | 8.0 | 8.0 | 8.0 | | | | COMP | 8.0 | 8.0 | 8.0 | N = NOISE |
| | | DISP | 4.1 | 4 . 1 | 4 . | | | | DISP | £.1 | 4.1 | 4.1 | = |
| | VEHICLE | SEN | > - | > | > | | | VEHICLE | SEN | > | > | > | 0E. |
| | Æ | 188 | 4 | 4 | 4 | | | VEH | 88 | 4 | 4 | 4 | M = MODE. |
| | | EMIS | L. | L | <u>.</u> | | | | EMIS | <u>.</u> | L. | L | |
| | | CODE | ۲ | * | . | | | | C00E | Ľ | ػ | 5 | G = GEAR. |
| | | 988 | ಕ | 4 | 9 | | | | 988 | 30 | 40 | 09 | |
| | | CYLS | 9-A | 4- 6 | N -6 | | | | CYLS | ۸-6 | N-6 | % | NOTE: |

* 50th Percentile Acceleration Technique

APPENDIX G

SUMMARY OF INDIVIDUAL CAR DATA

(RAW DATA AND WEATHER-CORRECTED DATA)

1981_CRC_ALTITUCE_PROGRAM_= 1961_VEHICLES

GROUP 1

RAW DATA

| 05.54 | | ELEU_MAX | | ~ | EERU_502 | * | | EBBSU_MA | Δ |
|---------------------------|------|----------|-------|-------------|----------|------|--------------|----------|------|
| Ω8 \$ V _ <u>\</u> Ω_• | LaAa | DENVER | DIEE | LaAa | DENVER | DIEE | LaAa | DENVER | DIEE |
| 10 | 87.5 | 63.0 | 4.5 | 87.5 | 78.0 | 9.5 | 87.5 | 83.0 | 4.5 |
| 11 | 88.0 | 81.0 | 7.0 | 68.0 | 80.0 | e.0 | 91.0 | 82.0 | 9.0 |
| 12 | 92.0 | 55.0 | 7.0 | 92.0 | 85.0 | 7.C | 93.0 | 85.C | 8.0 |
| 13 | 86.0 | 80.0 | 6.0 | E4.0 | 78.0 | 6.0 | 87. 0 | 82.0 | 5.0 |
| 14 | 86.0 | 8C.0 | 6.0 | 64.0 | 78.0 | 6.0 | 87.0 | 81.0 | 6.0 |
| 15 | 87.0 | 83.0 | 4 • C | 85.0 | 79.0 | 6.0 | ٤7.5 | 84.0 | 3.5 |
| 16 | 90.0 | 80.0 | 10.0 | 90.0 | 7E.0 | 12.0 | 91.0 | 80.0 | 11.0 |
| 17 | 95.0 | 82.0 | 13.C | 96.0 | 84.0 | 12.0 | 96.0 | 84.0 | 12.0 |
| 13 | 90.0 | 81.0 | 9.0 | 90.5 | 79.0 | 11.5 | 92.0 | 83.C | 9.0 |
| 19 | 85.0 | 0.03 | 5.0 | 65.0 | 78.0 | 7.0 | ٤7∙0 | 82.0 | 5.0 |
| MEAN | 88.7 | 81.5 | 7.2 | 58.2 | 79.7 | 8.5 | 9.98 | 82.6 | 7.3 |
| STD DEV | 3.1 | 1.7 | 2.€ | 3.9 | 2.6 | 2.5 | 3.2 | 1.5 | 2.9 |

GROUP 1

| | | EERU_MAX | | | EERU_50% | * | | EBRSU_MA | X |
|---------|------|----------|------|------|---------------|------|------|----------|------|
| DESV | | | | | | | | | |
| _NO. | Laka | DENVER | DIEE | LaAa | DENYER | DIEE | Laêa | DENYER | DIEE |
| 10 | 85.9 | 82.7 | 3.2 | 85.9 | 77.7 | 8.2 | 85.9 | 82.7 | 3.2 |
| 11 | 88.4 | 80.7 | 7.7 | 88.4 | 79.7 | 8.7 | 91.4 | 81.7 | 9.7 |
| 12 | 91.5 | 85.9 | 5.6 | 91.5 | 85.9 | 5.6 | 92.5 | 85.9 | 6.6 |
| 13 | 85.3 | 79.8 | 5.5 | £3.3 | 77 . e | 5.5 | 86.3 | 81.8 | 4.5 |
| 14 | 86.9 | 80.3 | 6.E | 84.9 | 78.3 | 6.6 | 87.9 | 81.3 | 6.6 |
| 15 | 86.5 | 84.3 | 2.2 | 64.5 | 80.3 | 4.2 | 87.0 | 85.3 | 1.7 |
| 16 | 89.6 | 79.7 | 9.9 | 89.6 | 77.7 | 11.9 | 90.6 | 79.7 | 10.9 |
| 17 | 94.1 | 83.0 | 11.1 | 95.1 | 85.0 | 10.1 | 95.1 | 85.0 | 10.1 |
| 18 | 89.0 | 80.8 | 8.2 | ٤9.5 | 78.8 | 10.7 | 91.0 | 82.8 | 8.2 |
| 19 | 84.3 | 80.9 | 3.4 | E4.3 | 78.9 | 5.4 | 86.3 | 62.9 | 3.4 |
| MEAN | 88.2 | ٤1.9 | 6.3 | 87.5 | 80.1 | 7.6 | 89.5 | 83.C | 6.4 |
| STD DEV | 3.0 | 2.1 | 2.9 | 3.8 | 3.0 | 2.6 | 3.2 | 2.0 | 3.2 |

^{* 50}th Percentile Acceleration Technique

1981_CRC_ALITIUDE_PROGRAM_= 1981_YEHICLES

GROUP 2

RAW DATA

| 20.57 | | EERULMAX | | ~~ | ELRU_50% | * | | EBRSU_MA | X |
|----------------|------|----------|------|---------------|----------|-------|------|----------|------|
| CB S V _ND. | L.A. | CENVER | DIEL | Lada | DENVER | DIEE | Leee | DENYER | DIEE |
| 20 | 90.0 | 67.0 | 3.0 | 90.0 | 88.0 | 2.C | 92.0 | 90.0 | 2.0 |
| 21 | 91.0 | 85.0 | 6.0 | 69.0 | 85.0 | 4 • C | 93.0 | 87.0 | 6.0 |
| 22 | 94.0 | 0.33 | 6.0 | 92.0 | 88.0 | 4.0 | 95.0 | 90.C | 5.0 |
| 23 | 88.0 | 67.0 | 1.0 | 88.0 | 84.0 | 4.0 | 90.0 | 88.0 | 2.0 |
| 24 | 91.0 | 88.0 | 3.0 | 91.0 | 88.0 | 3.0 | 92.0 | 90.0 | 2.0 |
| 25 | 90.0 | 86.0 | 2.0 | 59.0 | 88.0 | 1.C | 92.0 | 89.0 | 3.0 |
| 26 | 90.0 | 86.0 | 4.C | 90.0 | 86.0 | 4.0 | 91.0 | 0.88 | 3.C |
| 27 | 0.83 | 86.0 | 2.0 | € 7. 3 | 85.0 | 2.0 | 39.U | 88.0 | 1.0 |
| 28 | 91.0 | 89.0 | 2.0 | 91.0 | 87.0 | 4.0 | 93.0 | 89.5 | 3.5 |
| 29 | 93.0 | 91.5 | 1.5 | 93.0 | 91.0 | 2.0 | 97.0 | 92.0 | 5.0 |
| MEAN | 90.6 | 87.6 | 3.1 | 90.0 | 87.0 | 3.0 | 92.4 | 89.2 | 3.3 |
| STD DEV | 1.9 | 1.8 | 1.8 | 1.8 | 2.1 | 1.2 | 2.3 | 1.5 | 1.6 |

GROUP 2

| | | EERU_MAX | | | EERU_50%* | | | EBRSU_MAX | | |
|---------|------|----------|-------|------|-----------|-------|------|-----------|------|--|
| DBSV | | | | | | | | | | |
| _k2. | Laga | DELIVER | DIEE | Laés | DENXEB | DIEE | Le≜e | DENYER | DIEE | |
| 20 | 90.4 | 67.3 | 3.1 | 90.4 | 88.3 | 2.1 | 92.4 | 90.3 | 2.1 | |
| 21 | 90.3 | 85.6 | 4.7 | 66.3 | 85.6 | 2.7 | 92.3 | 87.6 | 4.7 | |
| 22 | 93.7 | 88.9 | 4.E | 91.7 | 88.9 | 2.8 | 94.7 | 90.9 | 3.8 | |
| 23 | 88.4 | 0.88 | G • 4 | 88.4 | 85.0 | 3.4 | 90.4 | 0.68 | 1.4 | |
| 24 | 90.1 | 87.7 | 2.4 | 90.1 | 87.7 | 2 • 4 | 91.1 | 89.7 | 1.4 | |
| 25 | 89.2 | 88.6 | 0.6 | 88.2 | 88.6 | -0.4 | 91.2 | 89.6 | 1.6 | |
| 26 | 90.0 | 85.2 | 4.8 | 90.0 | 85.2 | 4.8 | 91.0 | 87.2 | 3.8 | |
| 27 | 86.5 | 65.8 | 2.7 | 87.5 | 84.8 | 2.7 | 89.5 | 87.8 | 1.7 | |
| 28 | 91.7 | 88.2 | 3.5 | 91.7 | 86.2 | 5.5 | 93.7 | 88.7 | 5.0 | |
| 23 | 91.4 | 92.1 | -0.7 | 91.4 | 91.6 | -0.2 | 95.4 | 92.6 | 2.8 | |
| MEAN | 90.4 | £7.8 | 2.6 | 89.5 | 87.2 | 2.5 | 92.2 | 89.4 | 2.8 | |
| STD DEV | 1.6 | 2.0 | 2.0 | 1.6 | 2.2 | 1.9 | 1.9 | 1.7 | 1.4 | |

^{* 50}th Percentile Acceleration Technique

1981_CRC_ALITIUSE_PROGRAM_=_1981_VEHICLES

GROUP 3

RAW DATA

| CD CV | | EEEU_MAX | | | EBRU_50#* | | | EBRSU_MAX | | |
|--------------|------|----------|------|------|-----------|------|--------------|-----------|------|--|
| CBSV _L]_ | LaAa | DELIVER | DIEE | LaAs | DEBYER | DIEE | Laba | DENVER | DIEE | |
| 30 | £7.0 | 79.0 | 8.0 | £5.0 | 76.0 | 7.0 | 87. 0 | 81.0 | 6.0 | |
| 31 | 89.0 | 80.0 | 9.0 | 89.0 | 78.0 | 11.0 | 91.0 | 81.C | 10.0 | |
| 32 | 86.0 | 79.0 | 7.C | 85.0 | 79.0 | 6.0 | 29. 0 | 0.13 | 8.C | |
| 3 3 | 88.0 | 80.0 | €.0 | 89.0 | 80.0 | 9.0 | 90.0 | 82.0 | 8.0 | |
| 34 | 89.0 | 60.0 | 9.0 | 88.0 | 80.0 | 0.8 | 90.0 | 82.0 | 8.0 | |
| 35 | 89.0 | 80.0 | 9.C | 88.0 | 80.0 | 8.0 | 90. 0 | 82.0 | 8.C | |
| 36 | 90.0 | 60.0 | 10.0 | 90.0 | 76.0 | 12.0 | 92.0 | 80.0 | 12.0 | |
| 37 | 89.0 | 60.0 | 9.C | 88.0 | 80.0 | 8.C | 88.0 | 81.0 | 7.0 | |
| 38 | 0.33 | 80.0 | 8.C | 88.5 | 0.08 | 8.5 | 89.0 | 84.0 | 5.0 | |
| 39 | 94.0 | 84.0 | 10.0 | 94.0 | 84.0 | 10.0 | 95.0 | 85.0 | 9.0 | |
| MEAN | 85.9 | 80.2 | 8.7 | 88.5 | 79.7 | 8.8 | 90.1 | 82.0 | 6.1 | |
| STD DEV | 2.1 | 1.4 | 0.9 | 2.5 | 1.8 | 1.8 | 2.2 | 1.8 | 2.0 | |

GROUP 3

| | OBSVEERU_MAX | | | | EBRU_50%* | | | ERRSU_MAX | | |
|---------|--------------|--------|------|------|-----------|------|------|-----------|------|--|
| _%Q. | LaGa | DENYER | DIEE | Lada | DENVER | DIEE | Lada | DENYER | CIEE | |
| 30 | 87.0 | 79.2 | 7.8 | £5.0 | 78.2 | 6.8 | 87.0 | 81.2 | 5.8 | |
| 31 | 86.2 | 80.4 | 5.€ | 86.2 | 78.4 | 7.8 | 88.2 | 81.4 | 6.8 | |
| 32 | 85.0 | 79.7 | 5.3 | 84.0 | 79.7 | 4.3 | 88.0 | 81.7 | 6.3 | |
| 33 | 86.9 | 80.7 | 6.2 | £7.9 | 80.7 | 7.2 | 88.9 | 82.7 | 6.2 | |
| 34 | 88.2 | 80.7 | 7.5 | 87.2 | 80.7 | 6.5 | 89.2 | 82.7 | 6.5 | |
| 35 | 87.3 | 80.7 | 6.6 | 86.3 | 80.7 | 5.6 | 83.3 | 82.7 | 5.6 | |
| 36 | 87.7 | 80.7 | 7.0 | 87.7 | 78.7 | 9.0 | 89.7 | 80.7 | 9.0 | |
| 37 | 86.2 | 80.2 | 6.0 | £5.2 | 80.2 | 5.0 | 85.2 | 81.2 | 4.0 | |
| 38 | 87.6 | 80.7 | 6.9 | 88.1 | 80.7 | 7.4 | 88.6 | 84.7 | 3.9 | |
| 39 | 94.7 | 64.7 | 10.0 | 94.7 | 84.7 | 10.C | 95.7 | 86.7 | 9.0 | |
| MEAN | 67.7 | 80.8 | 6.9 | 87.3 | 80.3 | 6.9 | 86.9 | 82.6 | 6.3 | |
| STD DEV | 2.6 | 1.5 | 1.3 | 3.0 | 1.9 | 1.7 | 2.7 | 1.9 | 1.7 | |

^{* 50}th Percentile Acceleration Technique

1981_CR(_ALIJIUDE_PROGRAM_=_1981_VEHICLES

GROUP 4

RAW DATA

| 01.64 | C5SVEERU_MAX | | | | EBBU_50% | * | EBRSU_MAX | | |
|---------|--------------|--------|-------|------|----------|------|--------------|--------|-------------|
| | | 05,050 | 0155 | | DEMMED | DIEE | | DENVER | D. T. E. E. |
| _F0* | Laka | DEVAES | DIEE | Laba | DENYER | CIEE | Laba | | DIEE |
| 40 | 94.0 | 91.5 | 2.5 | 92.5 | 91.0 | 1.5 | 94.0 | 92.5 | 1.5 |
| 41 | 95.5 | 90.0 | 5.5 | 93.0 | 90.0 | 3.0 | 96.0 | 91.5 | 4.5 |
| 42 | 94.0 | 92.0 | 2.0 | 92.0 | 92.0 | 0.0 | 96.0 | 93.0 | 3.0 |
| 43 | 95.5 | 91.5 | 4.0 | 94.C | 92.5 | 1.5 | 96.0 | 92.0 | 4.0 |
| 44 | 94.0 | 92.0 | 2.0 | 94.0 | 92.0 | 2.0 | 97.0 | 93.0 | 4.0 |
| 45 | 91.5 | -90.0 | 1.5 | 89.0 | 89.0 | 0.0 | 92.0 | 91.5 | 0.5 |
| 46 | 94.0 | 90.0 | 4 • C | 92.0 | 90.0 | 2.0 | 94.0 | 91.0 | 3.0 |
| 47 | 94.5 | 90.0 | 4.5 | 94.0 | 89.0 | 5.0 | 97. 0 | 92.0 | 5.0 |
| 48 | 94.0 | 90.0 | 4.0 | 94.0 | 90.C | 4.0 | 96.0 | 91.0 | 5.0 |
| 49 | 94.0 | 90.0 | 4 • C | 93.5 | 89.0 | 4.5 | 94.0 | 91.0 | 3.0 |
| MEAN | 94.1 | 90.7 | 3.4 | 92.8 | 90.5 | 2.4 | 95.2 | 91.9 | 3.4 |
| STD DEV | 1.1 | 0.9 | 1.3 | 1.6 | 1.3 | 1.7 | 1.6 | 0.8 | 1.5 |

GROUP 4

| ESEU_MAX | | | | EBRU_50%* | | | EBRSU_MAX | | |
|----------|------|--------|------|-----------|--------|------|-----------|--------|------|
| OBSV | | | | | | | | | |
| _60. | Laka | DEPARS | DIEE | Laga | DENVER | DIEE | LaAa | DENXER | CIEE |
| 40 | 93.6 | 92.2 | 1.4 | 92.1 | 91.7 | 0.4 | 93.6 | 93.2 | 0.4 |
| 41 | 93.4 | 90.3 | 3.1 | 90.9 | 90.3 | 0.6 | 93.9 | 91.8 | 2.1 |
| 42 | 93.6 | 91.1 | 2.5 | 91.6 | 91.1 | 0.5 | 95.6 | 92.1 | 3.5 |
| 43 | 94.6 | 90.7 | 3.9 | 93.1 | 91.7 | 1.4 | 95.1 | 91.2 | 3.9 |
| 44 | 94.0 | 92.2 | 1.8 | 94.0 | 92.2 | 1.8 | 97.0 | 93.2 | 3.8 |
| 45 | 92.1 | 89.5 | 2.3 | 89.5 | 88.8 | 0.8 | 92.6 | 91.3 | 1.3 |
| 46 | 94.3 | 90.7 | 3.6 | 92.3 | 90.7 | 1.6 | 94.3 | 91.7 | 2.6 |
| 47 | 94.1 | 91.2 | 2.9 | 93.6 | 90.2 | 3.4 | 96.6 | 93.2 | 3.4 |
| 48 | 93.6 | 91.3 | 2.3 | 93.6 | 91.3 | 2.3 | 95.6 | 92.3 | 3.3 |
| 49 | 91.2 | 90.7 | 0.5 | 90.7 | 89.7 | 1.0 | 91.2 | 91.7 | -0.5 |
| MEAN | 93.5 | 91.1 | 2.4 | 92.2 | 90.8 | 1.3 | 94.5 | 92.2 | 2.3 |
| STD DEV | 1.0 | 0.8 | 1.0 | 1.5 | 1.0 | 0.5 | 1.8 | 0.8 | 1.5 |

^{* 50}th Percentile Acceleration Technique

GROUP 5

RAH DATA

| | ELSU_MAX | | | | EBPU_50#* | | | EBRSU_MAX | | |
|---------------|---------------|--------|------|-------|-----------|------|-------|-----------|------|--|
| _ <u>₽</u> ₽₽ | L.A. | DEMYER | DIEE | Laĝa | DENVER | DIEE | LaAa | DENYER | DIEE | |
| 50 | 100.0 | 91.0 | 9.0 | 101.C | 91.0 | 10.0 | 100.0 | 91.0 | 9.0 | |
| 51 | 88.0 | 81.0 | 7.0 | 88.0 | 80.0 | 6.0 | 87.5 | 82.0 | 5.5 | |
| 52 | 94.0 | 81.0 | 13.C | 94.0 | 81.0 | 13.0 | 94.0 | 84.0 | 10.0 | |
| 53 | 88.0 | 86.0 | 0.0 | £7.5 | 83.0 | 4.5 | 90.0 | 88.0 | 2.0 | |
| 54 | 94.0 | 85.0 | 9.0 | 94.0 | 84.0 | 10.0 | 96.0 | 86.0 | 10.0 | |
| 55 | 93.0 | 80.0 | 13.C | 94.0 | 80.0 | 14.0 | 95.0 | 82.C | 13.C | |
| 56 | £9.0 | 80.0 | 9.0 | 89.0 | 80.0 | 9.0 | 90.0 | 84.0 | 6.0 | |
| 57 | 96.0 | 82.0 | 14.0 | 96.0 | 82.0 | 14.C | 96.0 | 82.0 | 14.0 | |
| 58 | 96.0 | ε7.J | 11.0 | 99.0 | 86.0 | 11.0 | 99.0 | 89.0 | 10.0 | |
| 59 | έ7 . 0 | 50.0 | 7.0 | 2.68 | 79.C | 7.0 | 87.0 | 81.0 | 6.0 | |
| MEAN | 92.7 | £3.5 | 9.2 | 92.9 | 82.8 | 10.1 | 93.5 | 84.9 | 8.6 | |
| STD DEV | 4.5 | 4.0 | 4.1 | 5.1 | 3.9 | 3.1 | 4.6 | 3.4 | 3.7 | |

GROUP 5

| | ELEU_MAX | | | EBBU_50%* | | | EBRSU_MAX | | |
|------------|----------|--------|-------|-----------|--------|-------|---|--------|------|
| DESV | | CF 1 | חזרג | 1 4 | DENYER | DIEE | Lafa | DENVER | DIEE |
| عاتا الله | LeAe | DENVER | DIEE | Lada | 91.6 | 10.3 | 100.9 | 91.6 | 9.3 |
| 50 | 100.9 | 51.6 | 5.3 | 101.9 | | | | | |
| 51 | 87.6 | 61.7 | 5.9 | 87.6 | 80.7 | 6.9 | 87.1 | 82.7 | 4.4 |
| 52 | 92.3 | E1.4 | 10.9 | 92.3 | 81.4 | 10.9 | 92.3 | 84.4 | 7.9 |
| 53 | 86.1 | 56.8 | -2.7 | 25.6 | 83.8 | 1.8 | 86.1 | 88.5 | -0.7 |
| | 94.3 | 86.3 | 8.0 | 94.3 | 85.3 | 9.0 | 96.3 | 87.3 | 9.0 |
| 54 | | | | | 86.9 | 11.4 | 93.3 | 82.9 | 10.4 |
| 5 5 | 91.3 | €C.9 | 10.4 | 92.3 | | | , | 84.8 | 5.1 |
| 56 | 88.9 | 60.8 | 3.1 | 88.9 | 80.8 | 8.1 | 89•9 | | |
| 57 | 94.4 | E2.7 | 11.7 | 94.4 | 82.7 | 11.7 | 94.4 | 82.7 | 11.7 |
| 5 6 | 95.7 | 86.3 | 7.4 | 96.7 | 89.3 | 7.4 | 96.7 | 90.3 | 6.4 |
| 59 | £7.5 | 80.7 | 7.1 | 86.5 | 79.7 | 7.1 | 87∙6 | 81.7 | 6.1 |
| 59 | 67.5 | 00.1 | (• 1 | 00.5 | 1,74,1 | , , , | • | | |
| MEAN | 92.0 | 84.4 | 7.£ | 92.1 | 83.7 | 8.4 | 92.7 | 85.8 | 6.9 |
| | | | 4.1 | 5.0 | 4.0 | 3.0 | 4.5 | 3.5 | 3.6 |
| STD DEV | 4.5 | 4.1 | 4 • 1 | 2.0 | 7.0 | 200 | | | |

^{* 50}th Percentile Acceleration Technique

GROUP 6

RAW DATA

| 01.64 | | EEEU_WAX | | | LLLEBRU 508* | | | ESRSU_MAX | | |
|--------------|------|----------|------|------|--------------|------|------|-----------|------|--|
| _₽₽. _₽₽. | LaAa | LENYER | DIEE | Laba | DENXES | DILE | Laba | DENYER | DIEE | |
| 60 | 95.0 | 84.0 | 11.C | 95.0 | 84.C | 11.0 | 95.0 | 85.0 | 10.C | |
| 61 | 93.0 | 0.63 | 10.0 | 93.0 | 84.0 | 9.0 | 94.0 | 84.5 | 9.5 | |
| 62 | 92.0 | £5.0 | 7.0 | 92.0 | 85.0 | 7.0 | 94.0 | 87.0 | 7.0 | |
| 63 | 93.0 | 65.0 | 8.C | 92.0 | 65.0 | 7.0 | 94.0 | 87.0 | 7.C | |
| 64 | 93.0 | 66.0 | 7.0 | 94.0 | 86.0 | 8.0 | 93.0 | 88.0 | 5.0 | |
| 65 | 94.0 | 86.0 | 0.6 | 94.5 | 85.5 | 9.0 | 96.0 | 88.5 | 7.5 | |
| 66 | 93.0 | 82.0 | 11.0 | 93.0 | 84.C | 9.0 | 93.0 | 84.0 | 9.0 | |
| 67 | 90.0 | 83.0 | 7.0 | 90.0 | 83.0 | 7.0 | 94.0 | 85.0 | 9.0 | |
| 83 | 95.0 | 84.5 | 10.5 | 95.0 | 84.5 | 10.5 | 96.0 | 86.0 | 10.0 | |
| 69 | 94.0 | £3.0 | 11.0 | 95.0 | 83.0 | 12.0 | 94.0 | 0.88 | 11.0 | |
| MEAN | 93.2 | 64.2 | 9.1 | 93.4 | 84.4 | 9.0 | 94.3 | 85.8 | 8.5 | |
| STD DEV | 1.5 | 1.4 | 3.1 | 1.7 | 1.0 | 1.6 | 1.1 | 1.8 | 1.8 | |

GROUP 6

| 0.00 | DESVELEU_MAX | | | | E68U_508* | | | EBRSU_MAX | | |
|----------------------|--------------|--------|------|------|-----------|------|------|-----------|------|--|
| _₽Q + ₽62∧ | LeAs | LEBYES | DIEE | LaAa | DENVER | DIEE | LaAa | DENVER | DIEE | |
| 60 | 95.3 | 84.6 | 10.7 | 95.3 | 84.6 | 10.7 | 95.3 | 85.6 | 9.7 | |
| 61 | 93.4 | 82.9 | 10.5 | 93.4 | 83.9 | 9.5 | 94.4 | 84.4 | 10.0 | |
| 62 | 91.9 | 85.3 | 6.6 | 91.9 | 85.3 | 6.6 | 93.9 | 87.3 | 6.6 | |
| 63 | 93.0 | 65.3 | 7.7 | 92.0 | 85.3 | 6.7 | 94.0 | 87.3 | 6.7 | |
| 64 | 93.1 | 86.7 | 6.4 | 94.1 | 86.7 | 7.4 | 93.1 | 88.7 | 4.4 | |
| 65 | 93.9 | E6.3 | 7.6 | 94.4 | 85.8 | 8.6 | 95.9 | 88.6 | 7.1 | |
| 66 | 93.0 | 82.7 | 10.3 | 93.0 | 84.7 | 8.3 | 93.0 | 84.7 | 8.3 | |
| ι7 | 90.0 | 83.5 | 6.5 | 90.0 | 83.5 | 6.5 | 94.0 | 85.5 | 8.5 | |
| 6.5 | 95.4 | 85.2 | 10.2 | 95.4 | 85.2 | 10.2 | 96.4 | 86.7 | 9.7 | |
| 69 | 94.3 | £3.7 | 10.6 | 95.3 | 83.7 | 11.6 | 94.3 | 83.7 | 10.6 | |
| MEAN | 93.4 | £4.7 | 6.7 | 93.5 | 84.9 | 8.6 | 94.5 | 86.3 | ε.1 | |
| STO DEV | 1.6 | 1.4 | 1.5 | 1.8 | 1.0 | 1.8 | 1.1 | 1.8 | 1.9 | |

^{* 50}th Percentile Acceleration Technique

GROUP 7

RAW DATA

| 06 S V | EESU_MAX | | | ERRU_502* | | | EERSU_MAX | | |
|------------|----------|--------|------|-----------|--------|-------|-----------|--------|------|
| _00. | LaEs | DEPARS | DIEE | Lada | DENYER | DIEE | Laga | DENVER | DIEE |
| 70 | 92.0 | 85.5 | 6.5 | 91.0 | 83.0 | 8.0 | 96.0 | 88.5 | 7.5 |
| 71 | 94.0 | 85.0 | 9.0 | 94.0 | 83.0 | 11.0 | 97.0 | 86.5 | 10.5 |
| 72 | 99.0 | 96.0 | 3.€ | 99.0 | 96.0 | 3.C | 99.0 | 96.0 | 3.0 |
| 73 | 91.0 | 84.0 | 7.0 | 92.0 | 84.0 | 8.0 | 92.0 | 84.0 | 6.0 |
| 74 | 94.0 | 84.0 | 10.0 | 95.0 | 85.0 | 10.G | 95.0 | 85.0 | 10.0 |
| 75 | 59.0 | 93.0 | 0.0 | 98.0 | 93.0 | 5 • C | 99.0 | 93.0 | 6.0 |
| 76 | 99.0 | 8E.0 | 11.0 | 99.0 | 88.0 | 11.0 | 99.0 | 88.0 | 11.0 |
| 77 | 98.0 | 90.0 | 8.0 | 98.0 | 91.0 | 7.0 | 98.0 | 91.0 | 7.0 |
| 7 3 | 94.0 | 90.0 | 4.0 | 94.0 | 90.0 | 4.0 | 94.0 | 90.0 | 4.0 |
| 79 | ٤7.0 | 80.0 | 7.0 | 86.0 | 80.0 | 6.0 | 89.0 | 83.0 | 6.0 |
| MEAN | 94.7 | 87.6 | 7.2 | 94.6 | 87.3 | 7.3 | 95.8 | 88.5 | 7.3 |
| STO DEV | 4.1 | 4.8 | 2.5 | 4.2 | 5.1 | 2.8 | 3.4 | 4.1 | 2.7 |

GROUP 7

| | | ELEU_MAX | | | EBEU_5021* | | | ERRSU_MAX | | |
|---------|------|----------|------|-------|------------|------|------|-----------|------|--|
| CBSV | | | | | | | | | | |
| _04_ | LaAa | DEPXES | DIEE | Lesa | DENYER | DIEE | Laëa | DENYER | DIEE | |
| 70 | 92.0 | 86.4 | 5.6 | 91.0 | 83.9 | 7.1 | 95.0 | 89.4 | 6.6 | |
| 71 | 95.0 | 84.2 | 10.E | 95.0 | 82.2 | 12.8 | 98.0 | 85.7 | 12.3 | |
| 72 | 98.7 | 95.1 | 3.6 | 98.7 | 95.1 | 3.6 | 98.7 | 95.1 | 3.6 | |
| 73 | 90.4 | 83.2 | 7.2 | 91.4 | 83.2 | 8.2 | 91.4 | 83.2 | 8.2 | |
| 74 | 94.0 | 83.6 | 10.4 | 95.0 | 84.6 | 10.4 | 95.0 | 84.6 | 10.4 | |
| 75 | 98.9 | 93.7 | 5.2 | 97.9 | 93.7 | 4.2 | 98.9 | 93.7 | 5.2 | |
| 76 | 95.0 | 8៦.3 | 10.7 | 99.0 | 6.38 | 10.7 | 99.0 | 88.3 | 10.7 | |
| 77 | 96.4 | 90.3 | 8.1 | 98.4 | 91.3 | 7.1 | 98.4 | 91.3 | 7.1 | |
| 79 | 94.0 | E9.3 | 4.2 | 94.0 | 89.8 | 4.2 | 94.0 | 89.8 | 4.2 | |
| 79 | 87.1 | 79.5 | 7.3 | 86.1 | 79.8 | 6.3 | E9.1 | 82.8 | 6.3 | |
| MEAN | 94.8 | 87.5 | 7.3 | 94.7 | 87.2 | 7.4 | 95.9 | 88.4 | 7.4 | |
| STD DEV | 4.1 | 4.9 | 2.7 | 4 • 2 | 5.2 | 3.1 | 3.5 | 4.3 | 2.9 | |

^{* 50}th Percentile Acceleration Technique

1981 CRC ALTITUDE PROGRAM - 1981 VEHICLES

GROUP 8A (Cars Without Knocksensors)

RAW DATA

| 00.01 | | FBRU MAX | | | FBRU 50% | ** | FBRSU MAX | | | |
|--------------|-------------|----------|-------|------|----------|-------|-----------|--------|-------|--|
| OBSV. NO. | LA | Denver | Diff. | LA | Denver | Diff. | LA | Denver | Diff. | |
| 1 | 94.0 | 81.0 | 13.0 | 91.5 | 80.0 | 11.5 | 94.0 | 82.0 | 12.0 | |
| 2 | 88.0 | 82.0 | 6.0 | 88.0 | 82.0 | 6.0 | 92.0 | 85.0 | 7.0 | |
| 5 | 90.0 | 82.0 | 8.0 | 88.0 | 81.0 | 7.0 | 94.0 | 86.0 | 8.0 | |
| MEAN | 90.7 | 81.7 | 9.0 | 89.2 | 81.0 | 8.2 | 93.3 | 84.3 | 9.0 | |
| STD.DEV. | 3.1 | 0.6 | 3.6 | 2.0 | 1.0 | 2.9 | 1.2 | 2.1 | 2.7 | |

GROUP 8A

| OBSV. | FBRU MAX | | | FBRU 50%** | | | FBRSU MAX | | |
|----------|----------|--------|-------|------------|--------|-------|-----------|--------|-------|
| | LA | Denver | Diff. | LA | Denver | Diff. | LA | Denver | Diff. |
| 1 | 93.8 | 81.7 | 12.1 | 91.3 | 80.7 | 10.6 | 93.8 | 82.7 | 11.1 |
| 2 | 87.1 | 82.7 | 4.4 | 87.1 | 82.7 | 4.4 | 91.1 | 85.7 | 5.4 |
| 5 | 89.7 | 81.9 | 7.8 | 87.7 | 80.9 | 6.8 | 93.7 | 85.9 | 7.8 |
| MEAN | 90.2 | 82.1 | 8.1* | 88.7 | 81.4 | 7.3* | 92.9 | 84.8 | 8.1 |
| STD.DEV. | 3.4 | 0.5 | 3.9 | 2.3 | 1.1 | 3.1 | 1.5 | 1.8 | 2.9 |

^{*} Not statistically significant at the 95% confidence level.

^{** 50}th Percentile Acceleration Technique.

GROUP 88 (Cars With Knocksensors)

RAW DATA

| | FBRU | | | FBRU 50%+ | | | FBRSU | | |
|-----------------------------|---------|--------|-----------------|-----------|----------|--------------------|---------|---------|--------------------|
| 085V. NO. | LA | Denver | Diff. | LA | Denver | Diff. | LA | Denver | Diff. |
| | | | <u>Minimu</u> m | Octane | Requirer | ment | | | |
| 3 | 82.0 | 78.0 | 4.0 | 80.0 | 78.0* | 2.0 | 80.0 | 80.0 | 0.0 |
| 4 | 86.0 | 82.0 | 4.0 | 85.0 | 78.0 | 7.0 | 86.0 | 84.0 | 2.0 |
| 6 | 94.0 | 90.0 | 4.0 | 96.0 | 92.0 | 4.0 | 93.0 | 88.0 | 5.0 |
| MEAN | 87.3 | 83.3 | 4.0 | 87.0 | 82.7 | 4.3*** | 86.3 | 84.0 | 2.3*** |
| STD.DEV. | 6.1 | 6.1 | | 8.2 | 8.1 | 2.5 | 6.5 | 4.0 | 2.5 |
| Maximum Octane Requirement | | | | | | | | | |
| 3 | 95.0 | 89.0 | 6.0 | 93.0 | | 4.0 | 97.0 | 91.0 | 6.0 |
| 4 | 100.0** | 100.0 | 0.0 | 100.0** | | 0.0 | 101.0** | 101.0** | 0.0 |
| 6 | 100.0 | 95.0 | 5.0 | 100.0** | | 1.0 | 101.0 | 99.0 | 2.0 |
| MEAN | 98.3 | 94.7 | 3.7*** | 97.7 | 96.0 | 1.7 *** | 99.7 | 97.0 | 2.7*** |
| STD.DEV. | 2.9 | 5.5 | 3.2 | 4.0 | 6.1 | 2.1 | 2.3 | 5.3 | 3.1 |
| CRC E-15 Octane Requirement | | | | | | | | | |
| 3 | 93.0 | 88.0 | 5.0 | 92.0 | 88.0 | 4.0 | 93.0 | 89.0 | 4.0 |
| 4 | 99.0 | 98.0 | 1.0 | 98.0 | 98.0 | 0.0 | 101.0** | 101.0** | 0.0 |
| 6 | 97.0 | 93.0 | 4.0 | 98.0 | 93.0 | 5.0 | 97.0 | 95.0 | 2.0 |
| MEAN | 96.3 | 93.0 | 3.3*** | 96.0 | 93.0 | 3.0*** | 97.0 | 95.0 | 2.0 *** |
| STD.DEV. | 3.1 | 5.0 | 2.1 | 3.5 | 5.0 | 2.7 | 4.0 | 6.0 | 2.0 |

GROUP 8B WEATHER-CORRECTED DATA

| | FBRU | | | FBRU 50% | | | FBRSU | | |
|-----------------------------|------------------------|-----------------------|---------------------------|------------------------|-----------------------|-------------------|------------------------|-----------------------|-------------------|
| 085V. NO. | LA | Denver | Diff. | LA | Denver | Diff. | LA | Denver | Diff. |
| | | | <u>Minimu</u> m | Octane | Require | <u>nent</u> | | | ***** |
| 3 4 6 | 81.9 87.3 94.1 | 77.2 82.3 90.7 | 4.7 5.0 3.4 | 79.9 86.3 96.1 | 77.2 78.3 92.7 | 2.7 8.0 3.4 | 79.9 87.3 93.1 | 79.2 84.3 88.7 | 0.7 3.0 4.4 |
| MEAN STD.DEV. | 87.8 6.1 | 83.4 6.8 | 4.4 0.8 | 87.4 8.2 | 82.7 8.6 | 4.7*** 2.9 | 86.8 6.6 | 84.1 4.8 | 2.7*** 1.9 |
| | | | | | | | | | |
| 3 4 6 | 94.9 101.3 100.1 | 88.2 100.3 95.7 | | 92.9 101.3 100.1 | 88.2 100.3 99.7 | 4.7 1.0 0.4 | 96.9 102.3 101.1 | 90.2 101.3 99.7 | 6.7 1.0 1.4 |
| MEAN STD.DEV. | 98.8 3.4 | 94.7 6.1 | 4.0*** 2.9 | 98.1 4.5 | 96.1 6.8 | 2.0*** | 100.1 | 97.1 6.0 | 3.0*** 3.2 |
| CRC E-15 Octane Requirement | | | | | | | | | |
| 3 4 6 | 92.9 100.3 97.1 | 87.2 98.3 93.7 | 5.7 2.0 3.4 | 91.9 99.3 98.1 | 87.2 98.3 93.7 | 4.7 7.0 4.4 | 92.9 102.3 97.1 | 88.2 101.3 95.7 | 4.7 1.0 1.4 |
| MEAN STD.DEV. | 96.8 3.7 | 93.1 5.6 | 3,7 *** 1,9 | 96.4 4.0 | 93.1 5.5 | 3.4*** 2.1 | 97.4 4.7 | 95.1 6.6 | 2.4*** |

^{*} Requirement below lowest reference fuel, 78 RON assigned.

** Requirement above highest reference fuel, 100 RON FBRU or 101 RON FBRSU assigned.

*** Not statistically significant at the 95% confidence level.

* 50th Percentile Acceleration Technique.